EVALUATION OF CEMENTING EFFICIENCY OF QUATERNARY BLENDED HIGH STRENGTH SELF COMPACTING CONCRETE

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Abstract

The utilization of Supplementary Cementitious Materials (SCM) is well accepted because of the several improvements possible in the concrete composites, and due to the overall economy. Research work till date suggests that use of SCMs improve many of the performance characteristics of the hardened concrete. From the present investigations it is found that the compressive strength of metakaolin based high strength Self Compacting Concrete(SCC) depends both on the age and the percentages of replacement levels of Metakaolin, Micro Silica and Fly ash combination. The proposed work attempts to quantify the strength of Metakaolin, Silica fume and Fly ash combinationat the various optimum replacement levels and evaluate their efficiencies in SCC. In recent years replacement of cement with optimum combination of SCMs has emerged as a major alternative to conventional SCC and has rapidly drawn the concrete industry attention due to its cement savings, energy savings, and cost savings, environmental and socio-economic benefits. The present work proposes to report the results of an experimental study conducted to evaluate the synergic effects of Metakaolin, Micro Silica and Fly ash combination compressive strength of hardened Quaternary blended high strength SCC of M80 grades at different ages. The strength efficiency factor 'k' are evaluated usingBolomey's empirical expressions which are frequently used to predict the strength of concrete theoretically. The overall strength efficiency was found to be a combination of general efficiency factor, depending on the age and a percentage efficiency factor, depending upon the percentage of replacement of MetaKaolin, Silica fume and Fly ash combination. The experimental work on Micro Silica (MS) and MetaKaolin (MK) concrete found that the computed efficiency factor varied with pozzolan type, replacement level and age at 90 days. The value of k range from 1.71 to 1.84 for micro silica and MetaKaolin for 7 days. 1.16 to 1.11 for 28 days and 1.11 to 1.07 for 90 days in ternary blended SCC. The value of K quaternary blended SCC range from 1.88 for 7 days, 1.6 for 28 days and 1.19 for 90 days with 34% of waste industrial by product

Keywords: Self Compacting Concrete, Metakaolin, Micro Silica, Fly Ash, Efficiency Factor, Ternary Blended SCC, Quaternary Blended SCC

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1. INTRODUCTION

The Extensive research work for decades is in progress throughout the globe in concrete technology in finding alternative materials which can partially or fully replace ordinary Portland cement (OPC) and which can also meet the requirements of strength and durability aspects. Amongst the many alternative materials tried as partial cement replacement materials, the strength, workability and durability performance of industrial by products like fly ash (FA), blast furnace slag, microsilica, metakaolin, rice husk ash, etc., now termed as Supplementary cementitious materials (SCMs) are quite promising. Subsequently, these have led to the development of binary, ternary and quaternary blended concretes depending on the number of SCMs and their combinations used as partial cement replacement materials. The use of appropriately proportioned ternary or quaternary blended concretes allows the effect of one SCM to compensate for the inherent shortening of another. The one of the main objectives of this research was to investigate synergistic action of ternary selfcompacting concretes (SCC) on rheological properties,

strength and their cementing efficiencies in SCC. Several research studies have reported on the performance of Rice husk Ash (RHA) and Microsilica (MS) blended SCC. However, very limited research information was reported on the synergic action of Metakaolin and Microsilica in SCC for high performance concretes. The present investigations are aimed to study (1) the effect of synergic action of Metakaolin (MK), Microsilica (MS) and fly ash (FA) in SCC on Rheological behavior such as flowing, passing and filling ability; Strength properties and (2) their cementing efficiencies of FA, MS and MK in binary ,ternary and quaternary blended SCCs.

2. RESEARCH SIGNIFICANCE

Research work till date suggests that Metakaoline (MK), Microsilica (MS) improve many of the performance characteristics of the SCC such as strength, workability, permeability, and durability. From the present investigations it is found that the compressive strength of MK and MS based SCC depends both on the age and the percentage replacement level. It is felt that efficiency concept can be used to understand the behavior of MK and MS in SCC.In the present studies, Nan Su mix design method is adopted to determine the quantities of materials in kg per cu.m for high strength grade (M80) of blended Self Compacting Concrete (SCC). This paper presents a study on the behavior of MK and MS in SCC performance by evaluating the efficiency of MK and MS at different percentages of replacement for high strength grade (M80) grades in terms of efficiency factor "k". The strength efficiency factors for MK,MS and MK+FA,MS+FA dosages (in terms of percentage replacement) in SCC Mixes arecomputed based on the compressive strength of OPC only SCC mixes.

3. BOLOMEY'S EMPIRICAL EXPRESSION

The Bolomey's empirical expression frequently used to predict the strength of concrete is theoretically well founded when applied to hardened concrete.

Efficiency factors found from this strength equation are used to describe the effect of the MK and MS replacement. Efficiency factors are generally used to describe the impact of MK ,MS and FA replacement on the compressive strength of SCC Mixes.

The Bolomey's equation is:

S = A [(c/w)] + B (1) 'S' is the compressive strength in MPa, 'c' is the cement content in kg / m³, 'w' is the water content in kg/m³ and 'k' denotes efficiency factor.

By knowing the amounts of 'c', 'w' and the strength 'S' achieved for each slag dosage from the finally arrived experimental values, efficiency factor 'k' has been computed for each of the dosages.

Equation (1) has been shown to practically reduce to following two equations

$$\begin{split} S &= A \left[(\tilde{C}/W) - \tilde{0}.5 \right] & \dots \\ S &= A \left[(C/W) + 0.5 \right] & \dots \\ \end{split} \tag{2}$$

These two equations represent two ranges of concrete strengths and it is due to the often observed fact that a change in slope occurs at about w/p = 0.25, when P/W (powder-water ratio) is plotted against strength. However, it is found that the equation (2) is useful for most of the present day concretes when an analysis was done on test results available and also the extensive data published by Larrard who also mentions this equation in his famous book, on 'Concrete Mix Proportioning – A scientific approach'. Therefore, equation (2) can be generally used for re-proportioning. The value of constant 'A' can be found out for the given concrete ingredients, by considering a concrete mix of any w/c ratio.

For structural concrete, Equation (1) can be simplified as

S = A[(C/W) - 0.5] -- --(4) A strength efficiency factor, k, can then be computed using modified bolomey equation

$$S = A[(C+kP/W) - 0.5]$$
 ----- (5)

Where P is the amount of powder replaced by weight of cement. Thus, W/(C+kP) is the water/effective powderratio.

3.1 Cementing Efficiency Factor, K

This factor describes the mineral admixture's ability to act as cementing material recognizing that mineral admixture's contribution to concrete strength which comes mainly from its ability to react with free calcium hydroxide produced during cement hydration. The rate of this reaction, called as pozzolanic reaction (PR), when compared to cement hydration rate (CHR) determines the value of k. When k=1, both PR and CHR would be same and the water-binder ratios of concretes with and without MA could be almost same.

When k<1, PR would be slower than CHR and for equal strengths, the water-binder ratio of concrete with mineral admixture need to be less than that of concrete without mineral admixture and also, at same water-binder ratio, the strength of concrete with mineral admixture would be less than that of concrete without mineral admixture . In this case, the mineral admixture is less efficient than Portland cement in imparting strength to concrete. The GGBS has generally k<1 at early ages and k would reach a value of unity at later ages.

When k>1, PR would be faster than CHR and for equal strengths, the water-binder ratio of concrete with mineral admixture would to be more than that of concrete without mineral admixture .However, at similar water-binder ratios, the strength of concrete with mineral admixture would be more than that of concrete without mineral admixture. In this case, the mineral admixture is more efficient than Portland cement in imparting strength to concrete.

The contribution of MK and MS to any property of hardened concrete may be expressed in terms of efficiency factor, k. Based on the average compressive strength of the control SCC mix (100% OPC), 'A'value was calculated using Bolomey equation. Then Efficiency factors for MK,MS,MK+FA and MS+FA replaced SCC mixes were then determined using same bolomey equation. For this new material to be generally accepted by the building industry, a good durability must be proven also in quantitative terms. Therefore a big challenge for researchers within this field is to determine the strength efficiency of MK+FA and MS+FA in SCC.

4. EXPERIMENTAL INVESTIGATIONS

4.1 Determination Of Quantities Of Materials For

SCC Mixes

Based on Nan Su mix design method, quantities required for 1 cu.m are evaluated for high strength grade (M80) of binary, ternary and quaternary blended Self Compacting Concrete (SCC) made with SCMs such as Fly Ash (FA), Microsilica (MS) and Metakaolin(MK). Final quantities, for all SCC mixes considered, are assumed after several trial mixes on quantities computed using Nan Su mix design method subjected to satisfaction of EFNARC flow properties. This phase identifies the optimum proportions of fly ash, micro silica and met kaolin in binary, ternary and quaternary blended SCC for enhanced performance of SCC at all ages.

The following are the quantities of materials calculated using Nan Su mix design method for high strength grade

(M80) based Self Compacting Concrete (SCC) and also presented the final quantities of materials after various trial mixes.

,	Table-1: Quant	tities per 1 cu.	m for high streng	gth (M80) grade	SCC obtained u	using Nan	Su method of M	ix Design
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Grade of SCC Mix		Cement	Pozzolana (Fly ash)	Fine aggregate	Coarse aggregate	S.P.	Water	Water/Powder Ratio
M80	Quantity kg/m ³	644	13	821	778	10.6L	165 L	0.25

The amount of total powder (i.e., OPC+FA)(=450+410) for M80 grade blended SCC is 860 kg/m³.Using Nan Su method, for M80 grade blended SCC ,computed total weight of pozzolanic material (100% fly ash) is 13 kg/m³ (2% of total powder) .For the above powder content shown in

Table-1, flow properties are not achieved as per EFNARC guidelines, so several trail mixes were carried out to satisfy the flow properties. The following SCC mix proportions are arrived at after several trail mixes conforming EFNARC specifications for the required fresh properties.

Table-2: Final Quantities per 1 cu.m for high strength (M80) grade SCC mix after trail mixes

Grade of SCC Mix		Cement	Pozzolana (Fly ash)	Fine aggregate	Coarse aggregate	S.P.	Water	Water/Powder Ratio	
M80	Quantity kg/m ³	450	410	821	778	10.6L	215 L	0.25	

The following tables will illustrate the process of optimization of quantities of SCMs such as FA, MS and MK. For various binary, ternary and quaternary blended SCC mixes of high strength grade (M80), the tables demonstrate the strength achieved for various percentage replacements of pozzolanic materials considered in the study. The table-4 presents the final Optimal Quantities of

various grades of SCC mixes.Table -5 presents Compressive strength properties for Optimum SCC mixes made with combination of FA, MS and MK as SCMs. Table-6 presents total powder content and water powder ratios for various grades of blended SCC mixes. Table-7 to Table-9 presents Bolomey's Coefficient (A) for Bolomey's equation and Cementing Efficiency Factors.

Table 3: Trial Mixes for Fresh Properties High Strength M80 Grade SCC to opt	timize quantities of SCMS
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	Mix Designation	Repl	acemen (bw	t Percent p)*	tage	Slump I kg per d	Flow cu.m	V-Funnel		L-box
Mix No.		OPC	FA	MS	МК	Slump Flow Diameter Mm	T-50 Sec	T- 0Min sec	T-5 Min sec	Blocking ratio
C1	C100	100	-	-	-	707	3.22	63	8.3	0.96
в1	C52+FA48	52	48	-	-	780	2.7	5.2	6.8	0.84
T1	C52+FA43+MS5	52	43	5	-	770	3.1	5.4	7.2	0.86
T2	C52+FA38+MS10	52	38	10		765	3.8	5.6	7.8	0.87
T3	C52+FA33+MS15	52	33	15	-	740	4.2	6.1	12.1	0.96
T4	C52+FA28+MS20	52	28	20	-	700	4.6	7.2	14.1	0.98
T5	C52+FA43+MK5	52	43	-	5	770	2.9	5.1	6.9	0.84
T6	C52+FA38+MK10	52	38	-	10	760	3.4	4.9	8.8	0.82
T7	C52+FA33+MK15	52	33	-	15	710	3.8	5.3	10.8	0.94
T8	C52+FA28+MK20	52	28	-	20	705	4.2	5.6	11.4	0.96
Q1	C52+FA40+MS4+MK4	52	40	4	4	760	2.8	5.1	6.3	0.86
Q2	C52+FA36+MS6+MK6	52	36	6	6	730	3.2	4.8	8.1	0.94
Q3	C52+FA34+MS7+MK7	52	34	7	7	710	3.8	4.9	8.4	0.93

Mix No.	Mix Designation	Replacement Percentage(bwp)*					Quan kg per	tities cu.m		Achieved Strength(MPa)
		OPC	FA	MS	MK	OPC	FA	MS	MK	
C1	C100	100	-	-	-	860	-	-	-	84
B1	C52+FA48	52	48	-	-	450	410	-	-	59
T1	C52+FA43+MS5	52	43	5	-	450	370	40	-	67
T2	C52+FA38+MS10	52	38	10		450	327	83	-	74
T3	C52+FA33+MS15	52	33	15	-	450	284	126	-	86
T4	C52+FA28+MS20	52	28	20	-	450	241	169	-	89
T5	C52+FA43+MK5	52	43	-	5	450	370	I	40	65
T6	C52+FA38+MK10	52	38	-	10	450	327	-	83	71
T7	C52+FA33+MK15	52	33	-	15	450	284	I	126	84
T8	C52+FA28+MK20	52	28	-	20	450	241	I	169	87.3
Q1	C52+FA40+MS4+MK4	52	40	4	4	450	344	33	33	74
Q2	C52+FA36+MS6+MK6	52	36	6	6	450	310	50	50	88
Q3	C52+FA34+MS7+MK7	52	34	7	7	450	290	60	60	92.7

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Table-5: Final Optimal Quantities of various grades of SCC mixes *bwp** – *By weight of Total Powder content calculated from Nan Su mix design method*

Grade of SCC Mix	Mix No	Mix Designation (Values indicate percentage by weight of 'P'			Replacement % (bwp)* OPCFAMSMK			uan per FA	titie [•] cu. MS	es m MK	Total Powder Content 'P' kg	Water Powder Ratio W/P	
	C1	C100	100	-	-	-	860	-	-	-	860	0.25	
	B1	C52+FA48	52	48	-	-	450	410	-	-	860	0.25	
M80	T4	C52+FA28+MS20	52	28	20	-	450	241	169	-	860	0.25	
	T8	C52+FA28+MK20	52	28	I	20	450	241	I	169	860	0.25	
	Q3	C52+FA34+MS7+MK7	52	34	7	7	450	290	60	60	860	0.25	

Table-6: Determination of Hardened Properties for Optimum SCC mixes made with combination of FA, MS and MK as SCMs

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S.No.	Grade of SCC Mix	Mix No	Mix Designation (Values indicate percentage	Compressive Strength(MPa)							
			by weight of Total Powder)	3	7	14	28	60	90		
				days	days	days	days	Days	days		
1		C1	C100	31.5	42	61.2	78.3	81.2	84		
2		B1	C52+FA48	10.8	18.4	28.6	38.6	51.3	59		
3		T1	C52+FA43+MS5	15.3	21.4	31.4	47.2	63.2	67.1		
4		T2	C52+FA38+MS10	20.8	26.4	36.8	56	67.8	74.2		
5		T3	C52+FA33+MS15	21.8	38	47	66.2	77.1	86.3		
6		T4	C52+FA28+MS20	31.5	58.2	69.2	85.1	87.2	89.1		
7	M80	T5	C52+FA43+MK5	17.2	31.4	37.1	52.1	61.2	65		
8		T6	C52+FA38+MK10	25	33.2	42.1	59	66	71		
9		T7	C52+FA33+MK15	33.1	43.2	49.2	64	76.2	84.1		
10	1	T8	C52+FA28+MK20	38.3	61.2	56.2	65.6	74.2	87.3		
11		Q1	C52+FA40+MS4+MK4	16.4	28.2	37.2	43.2	68.6	74.4		
12		Q2	C52+FA36+MS6+MK6	34.2	49.1	62.1	74.4	82.4	88		
13		Q3	C52+FA34+MS7+MK7	41.4	62.1	68.1	85.1	89	92.7		

Table-7: Bolomey's Coefficients (A) for various grades of binary, ternary and quaternary blended SCC mixes

Grade of SCC Mix	Bolomey's Coefficients (A)										
	3 Days	7 days	14 days	28 days	60 days	90 days					
M80	9	12	17.48	22.37	23.2	24					

	Table	e-8: Ceme	nting Efficiency Factors at differen	t ages							
SNo	Grade of SCC Mix	Mix No	Mix Designation (Values indicate percentage	Efficiency Factors							
			by weight of Total Powder)	3	7	14	28	60	90		
				days	days	days	days	days	days		
1		C1	C100	-	-	-	-	-	-		
2	M80	T4	C52+FA28+MS20	1.01	1.71	1.24	1.16	1.13	1.11		
3		T8	C52+FA28+MK20	1.4	1.84	1.15	1.11	1.12	1.07		
4		Q3	C52+FA28+MS7+MK7	1.57	1.88	1.2	1.6	1.18	1.2		

5. DISCUSSIONS

- Table-1 presents the quantities per 1 cu.m for M80 ٠ grade SCC obtained using Nan Su method of Mix Design but for the powder quantities computed using this mix design method is not satisfying flow properties as per EFNARC guidelines, so several trail mixes were carried out to satisfy the flow properties. The final powder quantities for Standerd grade (M80) SCC mix are arrived at after several trail mixes conforming EFNARC specifications for the required fresh properties as shown in Table-2. From these final quantities, for various percentage replacement of cement by FA, MS, MK and their combinations are tried to optimize the quantities for binary, ternary and quaternary blended SCC mixes of grades considered. The percentage replacements, their corresponding desired strengths are tabulated in Table-3. In Table-4, final optimal quantities of various grades of SCC mixes along with their total powder content and water /powder ratios are mentioned. In Table-5, compressive strengths for various binary, ternary and quaternaryblended optimal SCC mixes are tabulated.
- For M80 grade SCC made with 100%OPC, EFNARC flow specifications and target compressive strength at 90 days can be accomplished. Equivalent compressive strengths can be achieved at 90 days for FA based binary, ternary and quaternaryblended SCC systems. In ternary blended M80 grade SCC systems, for OPC+FA+MS and OPC+ FA+MK combinations , compressive strengths comparable to that of 90 days target strength of 100% OPC high stength grade SCC can be achieved. For all the above binary, ternary and quaternarycombinations of SCMs, EFNARC flow specifications are satisfied.
- Compressive strengths are achieved early in MetaKaolinbased ternary and quaternaryblended SCC of all grades than in microsilica based ternary and quaternaryblended SCC. Due to synergy effect, the interaction of two or more admixtures is so that their combined effect is greater than the sum of their individual effects. In the other words, for reflecting synergic effect, the efficiency factor of Metakaolin, microsilica and fly ash combinationshould be higher in quaternaryblended SCC than in ternaryblended SCC system. For calculating the efficiency of Metakaolin, microsilica and fly ash combination in ternaryand quaternaryblended SCC, an equation has been proposed by author based on the principle of Bolomey's equation

for predicting the strength of concrete containing mineral admixtures. The efficiency factors evaluated can be used for proportioning of blended SCC.

- In ternary blended SCCcompressive strength of MS and MK based SCC mixes, K is in the range of 1.11 to 1.07 , which means that in a given SCC mix 1KG of MS or 1KG of MK based pozzolanic materials may replace 1.11. to 1.07 kg of cement without impairing the compressive strength. This may be valid, provided that the water content is kept constant. Bolomey's coefficients 'A' are calculated from the control mixes. Using computed 'A' value, calculate strength efficiency factors k at all ages for all percentage replacement levels of MS+FA , MK+FA, MS ,MK and FA combination in SCC.
- It is observed from efficiency factor is 1.11 for C52+FA28+MS20 and1.07 for C52+FA28+MK20 combinationsIn quaternary blended SCC it is observed from efficiency factor 1.19 for C52+FA34+MS7+MK7. It means that 1kg of MK or 1kg of MS based pozzolanic material may replaced by 1.19kg of cement quarternary blended mix is found to be more efficient because of high usage of waste byproduct FA(34%) with equal dosage of MS and MK

CONCLUSIONS

- [1]. Compressive strengths are achieved early in MetaKaolin based ternary and quaternary blended SCC.
- [2]. Due to synergy effect, the interaction of two or more admixtures is so that their combined effect is greater than thesum of their individual effects.
- [3]. For calculating the efficiency of MetaKaolin, Microsilica and fly ash combination in ternaryand quaternary blended SCC, an equation has been proposed by author based on the principle of Bolomey's equation for predicting the strength of concrete containing mineral admixtures.
- [4]. In ternary blended SCCcompressive strength of MS and MK based SCC mixes, K is in the range of 1.11 to 1.07, which means that in a given SCC mix 1KG of MS or 1KG of MK based pozzolanic materials may replace 1.11. to 1.07 kg of cement without impairing the compressive strength .This may be valid, provided that the water content is kept constant. Bolomey's coefficients 'A' are calculated from the control mixes. Using computed 'A' value, calculate strength efficiency factors k at all ages for all percentage

replacement levels of MS+FA, MK+FA, MS, MK and FA combination in SCC.

- [5]. It is observed from efficiency factor is 1.11 forC52+FA28+MS20 and 1.07 for C52+FA28+MK20 combinations.
- [6]. In quaternary blended SCC it is observed from efficiency factor 1.19 for C52+FA34+MS7+MK7.It means that 1kg of MK or 1kg of MS based pozzolanic material may be replaced by 1.19kg of cement.
- [7]. Quaternary blended mix is found to be more efficient because of high usage of waste byproduct FA(34%) with equal dosage of MS and MK
- [8]. Due to substantial saving in quantity of cement, ternary and quaternary blended MK, FA based SCC is considered as Green High Performance Concrete, because cement was replacing to maximum level with improvement of the performance properties. Therefore ternary and quaternary blended SCC reduces environmental and helps in sustainable development
- [9]. The findings of the present work endorses the recommendation that use of Microsilica and MetaKaolin in fly ash based SCC enhances both strength and replacement percentages of cement by mineral admixtures s found to be cost effective in terms of less cement usage, increased use of fly ash and also plays a major role in early strength development of FA based SCC
- [10]. In summary, the Microsilica and MetaKaolin based ternary and quaternary blended SCC gives better cohesiveness and solves problem of bleeding of ternary blended Microsilica based SCC and also adjusts the loss of workability which is a case of SCC blended with Micro Silica
- [11]. MetaKaolin based ternary and quaternary blended SCC reduces the setting times and imparts early strength when compared to ternary and quaternary blend SCC with Micro Silica
- [12]. It was observed that MetaKaolin based ternary and quaternary blended SCC requires less dosage of SP when compared to ternary and quaternary blended SCC with Micro Silica and which can be cost effective

REFERENCES

- [1]. De Silva, P.S. and F.P. Glasser, 1990. Hydration of cements based on metakaolin: thermochemistry. Advances in Cement Research, 3: 167-177.
- [2]. Ambroise, J., S. Maxmilien and J. Pera, 1994. Properties of MK blended cement. Advanced Cement Based Materials, 1: 161-168.
- [3]. Wild, S., J.M. Khatib and A. Jones, 1996. Relative strength pozzolanic activity and cement hydration in superplasticised MK concrete. Cement and Concrete Research, 26: 1537-1544.
- [4]. Wild, S., J.M. Khatib and M.J. Craythorne, 1997, Strength Development of Metakaolin Mortar. 5th International Conference on Modern Building Materials. Structures and Techniques, Lithuania, Vilnius Gediminas Technical University, 1: 58-63.
- [5]. Khatib, J.M., 2009. Low curing Temperature of Metakaolin Concrete. American Society of Civil

Engineers (ASCE) - Materials in Civil Engineering Journal, 21(8): 362-367.

- [6]. Khatib, J.M., B.B. Sabir and S. Wild, 1996. Some properties of Metakaolin Paste and Mortar, International Conference Concrete in the Service of Mankind: Concrete for Environment Enhancement and Protection, (Eds. R.K. Dhir and T.D. Dyer), Dundee, pp: 637-643.
- [7]. Sabir, B.B., S. Wild and J.M. Khatib, 1996. On the Workability and Strength Development of Metakaolin Concrete, International Conference - Concrete in the Service of Mankind: Concrete for Environment Enhancement and Protection, (Eds. R.K. Dhir and T.D. Dyer), pp: 651-662.
- [8]. Sabir, B.B., J.M. Kinuthia, J.M. Khatib and M.A. Wustoff, 2001. Relative Strength and Workability of Metakaolin - Fly Ash Concrete, Seventh International Conference on Modern Building Materials, Structures and Techniques, Lithuania, Vilnius Gediminas Technical University, 1: 43-51.
- [9]. Curcio, F., B.A. De Angelis and S. Pagliolico, 1998. Metakaolin as a pozzolanicmicro-filler for highperformance mortars, Cement and Concrete Research, 28(6): 803-809.
- [10]. Khatib, J.M. and S. Wild, 1996, Pore size distribution of metakaolin paste, Cement and Concrete Research, 1545-1553.
- [11]. Wild s,khatib JM,portlandite consumption in MetaKaolin cement pastes and mortars . cement concrete Res1997:27(I):137-46
- [12]. Wild S.Khatib JM, Jones A. Relative strength ,pozzolanic activity and cement hyderation in superplasticied metakaolin concrete . cement concrete Res 1996;26(10):1537-44
- [13]. Brooks JJ,Megat Johari , M.A, Mazloom M.Effect of admixtures on the setting times of high-strength concrete. Cement concrete compos 2000;22:293-301.
- [14]. FIP, State of the art report : condensed silica fume in concrete , Thomas Telford,London,1988.
- [15]. 15,V.G Papadakis,s.Tsimas,supplementary cementing materials in concrete: part 1:Efficiency and design , cem ,concr. Res, 32(2002) 1525-1532.
- [16]. A.M .Neville, properties of concrete, fourth ed., Addison Wesley Longman, Essex, UK.1996.

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