DEVELOPMENT OF CONDUCTING COPOLYMER BASED ON POLY (o-TOLUIDINE-co-2-AMINO 5 NAPHTHOL 7 SULPHONIC ACID): AN EFFICIENT MATERIAL FOR PROTECTION OF IRON IN HIGHLY CORROSIVE ENVIRONMENT

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Abstract
The report discusses the corrosion inhibition performance of highly soluble conducting copolymer based on Poly(o-Toluidine-co-2-Amino-5-Naphthol-7-Sulphonic Acid). The copolymer was synthesized by in situ chemical oxidative polymerization method by taking different molar concentration of comonomers. Characterization of synthesized copolymer was carried out by using FTIR, TGA and SEM measurement. The corrosion inhibition behaviour of the copolymer in 1.0 M HCl has been evaluated using Tafel Extrapolation method, electrochemical impedance spectroscopy (EIS) and weight loss measurements. The results showed that the copolymer consists of higher concentration of naphthyl amine comonomer exhibited the significant shifting in the corrosion potential and greater charge transfer resistance in highly aggressive medium such as 1.0 M HCl. Maximum corrosion inhibition efficiency up to 95% was obtained at 200 ppm concentration of the inhibitor. Moreover, the copolymer showed the larger degree of surface coverage onto the iron surface exhibits least corrosion rate, indicating the better protection of the iron in highly acidic medium.

Keywords: Conducting Copolymer, Corrosion Inhibitors, Tafel Plots, Impedance Spectroscopy.

1. INTRODUCTION
 Metals such as iron and steel are widely used as the constructional material in most of the major industries mainly in power plant, chemical plants, food, petroleum, electrochemical industries water and oil pipelines etc due to their outstanding mechanical properties and low cost. The major problem of these metals is that they are dissolved/degradation in acidic, aqueous and alkaline medium. Corrosion of iron and steel in acidic aqueous solutions is one of the major areas of concern for many industries where acids are extensively used for various applications such as acid cleaning, acid pickling, descaling, and oil well acidizing. Due to the corrosive nature of the acid solution, the materials of manufacture are being corroded easily. Therefore, it is very important to introduce such inhibitors which can prevent the metals from dissolution and degradation, and also reduce acid consumption [1-3]. Among the several methods of corrosion protection such as cathodic protection [1,2], anodic protection [3] and coating [4], the use of chemical inhibitors is found to be the most efficient method for protection of metals from corrosion. A corrosion inhibitor is a chemical additive which when added to a corrosive aqueous environment reduces the rate of metal dissolution. Use of acid inhibitors such as organic compounds including sulfur, nitrogen and oxygen atoms is well known method for corrosion protection. The inhibiting action applied by organic compounds on the dissolution of metallic species is related to interactions by adsorption between the inhibitors and the metal surface [4-7]. High electron density of the heteroatom such as nitrogen and sulphur atoms present in hetero compounds facilitates the organic molecule to get adsorbed onto the metal surface [7].

Moreover, the high-quality inhibitors should have the properties like cost effective, high inhibition efficiency, low toxicity and easy production and better solubility in common organic solvents [6, 7].

Conducting polymers such as polyaniline, polypyrrole and their copolymers found to be highly efficient inhibitors for protection of metal from corrosion due to presence of \( \pi \) electrons, quaternary nitrogen atom and large molecular size [8-10].

In the last two decades; conducting polymer based inhibitors has been playing an important role to inhibit the corrosion of steel in highly corrosive conditions [3-7]. Among all conducting polymers, polyaniline has a special representation due to easy synthesis, environmental stability, simple non-redox doping by protonic acids. Though, the commercial utilization of most of the applications based on polyaniline is very much related to the ease of its
processability and solubility. Solubility of polyaniline in common organic solvents like ethanol, methanol or water is the most important requirement for its use as a corrosion inhibitor; however polyaniline is insoluble in these solvents. On the basis of literature it was found that the use of alkyl-substituted polyaniline and their copolymers, better solubility in organic solvents like ethanol and methanol can easily be achieved because of the stereo-electronic effects of the substituent on the torsion angle [11-13]. Bhandari et al reported corrosion inhibition behavior of poly(aniline-co-2-isopropylamine), on the basis of literature, it was observed that copolymers based on aniline and alkyl substituted aniline were found to be better corrosion inhibitors as compared to polyaniline [5]. In addition, Bhandari et al also reported the corrosion inhibitor behavior of conducting copolymer based on poly(Aniline-co-1-amino-2-naphthol-4-sulphonic acid). Copolymers based on naphthyl amine derivatives bearing different functional group like –OH, NH₂ were found to be highly efficient corrosion inhibitors in strong acidic medium [14, 15].

Therefore, the present work deals with the development and evaluation of highly soluble conducting copolymer based on Poly(o-Toluidine-co-2-Amino-5-Naphthol-7-Sulphonic acid) for protection of iron in highly corrosive acid medium (i.e.1.0 M HCl). To the best of our knowledge, there was no report in the literature related to the corrosion inhibition behavior of conducting copolymer based on Poly(o-Toluidine-co-2-Amino-5-Naphthol-7-Sulphonic acid). The corrosion inhibition behavior of synthesized copolymer was evaluated using Tafel weight loss method, polarization and electrochemical impedance spectroscopy (EIS) measurements.

2. EXPERIMENTAL

2.1 Materials

Ortho-toluidine (OT) and 2-Amino-5-Naphthol-7-Sulphonic acid (ANS) (Loba Chemie, India) was used after distillation. Ammonium peroxysulphate (APS) (Merck, India) and p-Toluene sulphonic acid (PTSA) were purchased from Aldrich, India. Aqueous solutions were prepared from the double distilled water having specific resistivity of 1MΩ-cm.

2.2 Synthesis of Poly (o-Toluidine-co-2-Amino-5-

Naphthol-7-Sulphonic Acid)

Conducting copolymer Poly(o-Toluidine-co-2-Amino-5-Naphthol-7-Sulphonic acid) have been synthesised by chemical oxidative polymerization using p-Toluene sulphonic acid (PTSA) as a dopant. For preparation of Poly(o-Toluidine-co-2-Amino-5-Naphthol-7-Sulphonic acid), different molar ratio of comonomers such as (0.1 M o-Toluidine and 0.01 M 2-Amino-5-Naphthol-7-Sulphonic acid) and (0.1 M o-Toluidine and 0.1 M 2-Amino-5-Naphthol-7-Sulphonic acid) was taken in 0.2 M PTSA solution. The copolymerization was initiated by the drop wise addition of aqueous solution of 0.1 M ammonium peroxydisulfate (APS) which acts as an oxidant. The copolymerization was carried out at a temperature of 0-3 °C for a period of 4-6 h. The synthesized copolymers was isolated from reaction mixture by filtration and washed with distilled water to remove oxidant and oligomers and followed by drying in the vacuum oven at 60°C. Synthesised Poly(o-Toluidine-co-2-Amino-5-Naphthol-7-Sulphonic acid) having different molar ratio of comomers (0.1 M o-Toluidine and 0.01 M 2-Amino-5-Naphthol-7-Sulphonic acid) and (0.1 M o-Toluidine and 0.1 M 2-Amino-5-Naphthol-7-Sulphonic acid) was designated as POT-co-ANS1 and POT-co-ANS2 respectively.

3. CHARACTERIZATION

The structure of the copolymer was characterized by Fourier Transform Ntered (FTIR) Spectrometer (Nicolet 5700 FTIR, USA) in KBr pellets in the range of 400-4000 cm⁻¹. TGA (Metttler Toledo TGA/SDTA 851e, Switzerland) was used to investigate the thermal stability of copolymers in nitrogen atmosphere. A heating rate of 10°C/min and a sample size (in the form of fine powder) of 10±2 mg were used in each experiment. Morphology was observed using Scanning Electron Microscopy (SEM; Leo S-440, Germany).

3.1 Study of the Corrosion- Inhibition Performance of Inhibitors

The corrosion inhibition study was carried out at room temperature in aqueous solution of 1.0 M HCl by using electrochemical impedance spectroscopy measurements and potentiotodynamic polarization technique. Experiments were carried out in a usual three electrode cell system using Autolab Potentiostat/ Galvanostat, PGSTAT100 (Nova Software). Pure mild steel of dimension 1 cm x 1 cm was employed as working electrode embedded in araldite epoxy, Platinum as counter electrode and saturated calomel electrode (SCE) as reference electrode. The cleaning of the working iron electrode was carried out by fine emery papers and then the mild steel electrodes were thoroughly cleaned with trichloroethylene and acetone to remove the extra impurities from the metal surface. The linear Tafel segments to the anodic and cathodic curves (-0.2 to +0.2 V versus corrosion potential) were extrapolated to corrosion potential to obtain the corrosion current densities. The corrosion current density (i corr (A/cm²)) was calculated with the Stern-Geary equation [16]. The corrosion inhibition efficiency (% I.E.) was determined from the measured i corr (corrosion current densities without addition of inhibitor) (i corr) and corrosion current densities with the addition of various concentrations of inhibitor (i corr) values by using the following relationship;

$$\text{I.E.}(\%) = \frac{i_{corr}^0 - i_{corr}^1}{i_{corr}^0} \times 100 \quad (1)$$

The corrosion inhibition efficiency was also calculated by measured charge transfer resistance Rct value in electrochemical impedance study (EIS), using Frequency Response Analyser (FRA) 2.3 where AC signals of 10 mV
amplitude and a frequency spectrum from 10 KHz to 10 Hz were applied. In impedance studies, the corrosion inhibition efficiency was calculated by measured charge transfer resistance \( R_{ct} \) value with following relationship:

\[
I.E.(\%) = \frac{R_{ct}^\infty - R_{ct}^\infty}{R_{ct}^\infty} \times 100 \tag{2}
\]

where, \( R_{ct}^\infty \) and \( R_{ct}^\infty \) are the charge transfer resistance in the absence and in presence of inhibitors respectively. The Nyquist plots obtained by impedance measurements showed single semicircle curves which indicate the occurrence of a single charge transfer reaction. The curves show the depressed semicircle indicating the activation controlled nature of the reaction process with micro roughness at the surface of iron electrode during corrosion [17]. The impedance data were analysed with the equivalent circuit as shown in the Fig. 1,

![Fig-1: Electrical Equivalent circuit of EIS](image)

where \( R_{ct} \) is the charge transfer resistance, \( R_s \) is the solution resistance and CPE is the constant phase element of double layer capacitance (\( C_{dl} \)). The \( C_{dl} \) has been estimated from the impedance value of the frequency (\( f_{max} \)) having maximum imaginary component with Nyquist plot by using following relationship [18];

\[
C_{dl} = \frac{1}{2\pi f_{max} R_{ct}} \tag{3}
\]

and the surface coverage (\( \theta \)) by the inhibitor molecule can be calculated by using the following relationship;

\[
\theta = \frac{C_{dl}^0 - C_{dl}^\infty}{C_{dl}^\infty} \tag{4}
\]

where \( C_{dl}^0 \) and \( C_{dl}^\infty \) are the double layer capacitance in the absence and in presence of inhibitors respectively.

### 3.2 Weight Loss Method

The weight loss methods have also been performed for corrosion study. The iron specimens of dimension 4 x 3 cm\(^2\) were weighed in an electronic balance with an accuracy of 0.1 mg, before immersion in HCl medium. Iron specimens have been tested for same span of time by immersing the samples in aqueous solution of 1.0 M HCl with and without addition of inhibitors after 20 days. After 20 days of immersion specimens were removed from the tested solution, washed thoroughly with distilled water followed by acetone and dried with air, then weighed again. The corrosion inhibition performance was checked visually and using calculation of the weight loss. Weight loss is expressed as the loss in the weight per unit area or per unit area per unit time (g cm\(^{-2}\) h\(^{-1}\)) as follows:

\[
WL = \frac{w_0 - w_t}{a t} \tag{5}
\]

where, \( w_0 \) = initial weight of the sample before immersion (g); \( w_t \) = weight of the sample after immersion (mg); \( a \) = surface area (cm\(^2\)) of specimen; \( t \) = end time (h) of each experiment.

### 4. RESULTS AND DISCUSSION

#### 4.1 FTIR Spectra

Fig. 2 shows the FTIR spectra of POT-co-ANS, band around 815-820 cm\(^{-1}\) is due to the out of the plane C-H bending vibrations and is indicative of the para coupling i.e. the polymerization occurs at 1,4- position in o-toluidine ring. The band around 757 cm\(^{-1}\) and 750 cm\(^{-1}\) is due to the out-of-plane –CH\(^\prime\) bending of 1, 2, 4-trisubstituted ring due to o-toluidine ring in copolymer chain. The band at 1040 cm\(^{-1}\) in corresponds to S=O stretching mode of the -SO\(_3\) group of PTSA. Copolymer of OT and ANS also showed a characteristic band at 1350 cm\(^{-1}\), due to presence –OH in plane bending. Characteristic band at 3234 cm\(^{-1}\) is due to hydrogen bonded –OH and –NH\(_2\) groups.

![Fig-2: FTIR spectra of (a) POT-co-ANS1 and (b) POT-co-ANS2](image)
4.2 Thermo Gravimetric Analysis

Fig. 4 shows the thermo-gravimetric curves (TGA) of POT-co-ANS. The sample was heated from 25 to 700°C under a constant heating rate of 10°C/min and inert atmosphere of nitrogen gas.

It was observed that conducting copolymers POT-co-ANS1 and POT-co-ANS2 showed an excellent thermal stability in the range of 250 to 270°C. The TGA curve of copolymer indicates that first weight loss at 100-110°C is attributed to the loss of water and other volatile species. The weight loss in the second step at about 250-270°C onwards involves the loss of dopant ions as well as onset of degradation of copolymer backbone.

4.3 Morphological Characterization of Copolymers

Fig. 5 shows the scanning electron microscopy (SEM) images of copolymers (POT-co-ANS1 and POT-co-ANS2). SEM image of copolymer consists of 0.1 M OT and 0.01 M ANS showed rock like morphology. On increasing the molar concentration of ANS comonomer, change the morphology of copolymer (POT-co-ANS2) to tubular shape as shown in Fig.5, which indicates that the tube like shape of the copolymer is due the incorporation of higher concentration ANS in copolymer matrix.

4.4 Solubility

On the basis of literature it was observed that polyaniline doped with dopant such as inorganic protic acid like HCl is found to be slightly insoluble in organic solvents. However, polyaniline doped with organic aromatic sulphonic acid dopants like p-toluene sulphonic acid and Dodecyl benzene sulphonic acid is soluble in chloroform, DMF, DMSO but rather insoluble in common organic solvents like water and alcohols [19].

On the other hand it was found that the copolymers based POT-co-ANS doped with PTSA was found to be soluble in common organic solvents such as methanol and ethanol. Copolymers POT-co-ANS1 showed upto 60 % and POT-co-ANS2 exhibited upto 90 % solubility in alcohol. Solubility of synthesized copolymers is better than polyaniline due to the steric hindrance brought about by the introduction of different substituents at the aniline and naphthalene rings. Higher concentration of ANS monomer in copolymer chain also plays an important role to improve solubility of copolymer in organic solvents. For corrosion studies by electrochemical methods, the methanol medium was selected as a solvent for corrosion studies as all the corrosion studies for iron were carried out in aqueous solution of 1.0 M HCl, since methanol is miscible with aqueous medium, it has not affected the overall performance of the corrosion inhibition studies.
5. CORROSION INHIBITION STUDY

5.1 Tafel Extrapolation Measurement

Fig.6 shows the Tafel polarization curve for iron in 1.0 M HCl with the addition of various concentrations of inhibitors (POT-co-ANS) in methanol. The copolymers were highly soluble in various organic solvents such as ethanol, methanol DMSO and NMP, but in the present studies, we have selected methanol as a solvent due to its good solubility in aqueous solution of HCl.

Table-1: Tafel parameters for iron in 1.0 M HCl containing different concentration of inhibitors

<table>
<thead>
<tr>
<th>Inhibitor’s name</th>
<th>Inhibitor’s concentration</th>
<th>$E_{\text{corr}}$ (Volts)</th>
<th>$i_{\text{corr}}$ (μA/cm$^2$)</th>
<th>I.E (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Without inhibitor</td>
<td>---</td>
<td>-0.548</td>
<td>918</td>
<td>--</td>
</tr>
<tr>
<td>POT-co-ANS1</td>
<td>50</td>
<td>-0.505</td>
<td>430</td>
<td>53</td>
</tr>
<tr>
<td></td>
<td>100</td>
<td>-0.480</td>
<td>265</td>
<td>71</td>
</tr>
<tr>
<td></td>
<td>150</td>
<td>-0.460</td>
<td>206</td>
<td>76</td>
</tr>
<tr>
<td></td>
<td>200</td>
<td>-0.445</td>
<td>165</td>
<td>82</td>
</tr>
<tr>
<td>POT-co-ANS2</td>
<td>50</td>
<td>-0.485</td>
<td>251</td>
<td>73</td>
</tr>
<tr>
<td></td>
<td>100</td>
<td>-0.466</td>
<td>190</td>
<td>79</td>
</tr>
<tr>
<td></td>
<td>150</td>
<td>-0.440</td>
<td>149</td>
<td>84</td>
</tr>
<tr>
<td></td>
<td>200</td>
<td>-0.421</td>
<td>50</td>
<td>95</td>
</tr>
</tbody>
</table>

The Tafel curves expose that the corrosion potential ($E_{\text{corr}}$) value of iron in 1.0 M HCl was found to be -0.548 V without addition of inhibitors. Addition of different concentration of inhibitors POT-co-ANS1 showed a remarkable potential shift from -0.548 V to -0.455 V versus SCE in the corrosion potential ($E_{\text{corr}}$), relative to the value of the iron without inhibitors. The positive shift in $E_{\text{corr}}$ indicates the significant inhibition performance of iron in presence of inhibitor in acidic medium. Moreover, corrosion current density ($i_{\text{corr}}$) value of the iron electrode was also reduced significantly by using POT-co-ANS1 inhibitor. The corrosion kinetic parameters derived from these curves are given in the Table 1. It is clear from the Table 1, that the corrosion current density ($i_{\text{corr}}$) decreased from 918 μA/cm$^2$ iron electrode (without inhibitor) to 265 μA/cm$^2$ with the addition of 100 ppm concentration of POT-co-ANS1 copolymer. On increasing the concentration of POT-co-ANS1 at 200 ppm in acidic medium, the $i_{\text{corr}}$ value decreased to 165 μA/cm$^2$. Hence the addition of 200 ppm concentration of copolymer based on 0.1M OT and 0.01 M ANS, the $i_{\text{corr}}$ value decreased from 918 μA/cm$^2$ for inhibitor-free solution to 165 μA/cm$^2$ to yield a 82 % corrosion inhibition efficiency. While in copolymer based on 0.1M OT and 0.1 M ANS (POT-co-ANS2), the $i_{\text{corr}}$ value decreased from 918 μA/cm$^2$ for inhibitor-free solution to 50 μA/cm$^2$ on addition of 200 ppm concentration. Corrosion inhibition efficiency of iron on addition of 200 ppm solution of POT-co-ANS2 was found to 95 % as shown in Fig. 6. The copolymer composition based on POT-co-ANS2 showed better inhibition efficiency than that of copolymer POT-co-ANS1.

5.2 Electrochemical Impedance Spectroscopy (EIS)

The Nyquist representations of the impedance behaviour of iron in 1.0 M HCl with and without addition of various concentrations of inhibitors are shown in Fig.7. The existence of single semicircle showed the single charge transfer process during the dissolution of metal. It was observed that the addition of copolymers increases the value of charge transfer resistance ($R_{\text{ct}}$) and reduces the interfacial double layer capacitance ($C_{\text{dl}}$).
The decrease in $C_{dl}$ value revealed the increase in thickness of electrical double layer. Moreover, the increase in $R_{ct}$ value is attributed to the formation of protective film on the metal/solution interface [20]. The $R_{ct}$ and $C_{dl}$ values derived from these curves are given in the Table 2. It is clear from the Table 2 that the charge transfer resistance ($R_{ct}$) value of mild steel electrode increased from 12 $\Omega$ cm$^2$ (without addition of inhibitor) to 78 $\Omega$ cm$^2$ with the addition of 100 ppm concentration of POT-co-ANS1. Further addition of 200 ppm concentration of POT-co-ANS1, $R_{ct}$ value found to be increased from 100 $\Omega$ cm$^2$ to 150 $\Omega$ cm$^2$ The interfacial double layer capacitance ($C_{dl}$) values derived from the Nyquist plot are given in the Table 2.

Table-2: Electrochemical Impedance parameters for iron in 1.0 M HCl containing different concentration of inhibitors

<table>
<thead>
<tr>
<th>Inhibitor’s Name</th>
<th>Inhibitor’s concentration</th>
<th>$R_{ct}$ ($\Omega$ cm$^2$)</th>
<th>$C_{dl}$ ($\mu$F cm$^{-2}$)</th>
<th>LE (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Without inhibitor</td>
<td>---</td>
<td>12</td>
<td>354</td>
<td>--</td>
</tr>
<tr>
<td>POT-co-ANS1</td>
<td>50</td>
<td>60</td>
<td>142</td>
<td>80</td>
</tr>
<tr>
<td></td>
<td>100</td>
<td>78</td>
<td>106</td>
<td>85</td>
</tr>
<tr>
<td></td>
<td>150</td>
<td>95</td>
<td>92</td>
<td>87</td>
</tr>
<tr>
<td></td>
<td>200</td>
<td>101</td>
<td>65</td>
<td>88</td>
</tr>
<tr>
<td>POT-co-ANS2</td>
<td>50</td>
<td>78</td>
<td>103</td>
<td>85</td>
</tr>
<tr>
<td></td>
<td>100</td>
<td>100</td>
<td>64</td>
<td>88</td>
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<tr>
<td></td>
<td>150</td>
<td>125</td>
<td>55</td>
<td>90</td>
</tr>
<tr>
<td></td>
<td>200</td>
<td>150</td>
<td>37</td>
<td>92</td>
</tr>
</tbody>
</table>

The $C_{dl}$ values were found to decrease from 354 $\mu$F cm$^{-2}$ for inhibitor free solution to 142 $\mu$F cm$^{-2}$, 106 $\mu$F cm$^{-2}$, 92 $\mu$F cm$^{-2}$ and 65 $\mu$F cm$^{-2}$ with the addition of 50 ppm, 100 ppm, 150 ppm and 200 ppm concentration of POT-co-ANS1 respectively. While in case of POT-co-ANS2, $C_{dl}$ values were found to decrease from 354 $\mu$F cm$^{-2}$ for inhibitor free solution to 37 $\mu$F cm$^{-2}$ with the addition of 200 ppm concentration. Moreover, the degrees of surface coverage of iron by these copolymers at different concentration of inhibitors have also been calculated, which revealed that copolymer prepared by using higher concentration of ANS i.e.0.1 M, showed the greater surface coverage onto the iron electrode. The large surface coverage upto 90 % shown by POT-co-ANS2 at 200 ppm, indicates the greater adsorption of this inhibitor onto iron surface.

The mechanism of corrosion inhibition may be explained on the basis of adsorption behaviour [20, 21]. Fig. 8 shows the adsorption isotherms of POT-co-ANS2 copolymer. Data are tested graphically by fitting to various isotherms. A straight line was obtained on plotting the inhibitor concentration $C_{inh}$ vs ($C_{inh}/\theta$) for the copolymers. The linear relationship of the plots showed that these copolymers inhibited the corrosion of iron in acid solution i.e. 1.0 M HCl by surface coverage of inhibitor adsorption consistent with Langmuir adsorption isotherm.

5.3 Weight Loss Measurements

Table 3 shows the values of the weight loss from iron samples during the immersion test for 20 days in 1.0 M HCl solution. The results revealed that iron samples were more protectable in presence of POT-co-ANS2 inhibitors as compared to POT-co-ANS1 samples in same immersion time and same concentration.

Table -3: Weight loss study for iron in presence of inhibitors in 1.0 M HCl

<table>
<thead>
<tr>
<th>Inhibitor’s name</th>
<th>Inhibitor conc. (ppm)</th>
<th>Initial Weight of iron(mg) before immersion</th>
<th>Final weight after immersion (mg)</th>
<th>Weight loss (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Without inhibitor</td>
<td>-</td>
<td>32550.5</td>
<td>19520.2</td>
<td>40.00</td>
</tr>
<tr>
<td>POT-co-NS1</td>
<td>50</td>
<td>32780.2</td>
<td>20560.6</td>
<td>37.27</td>
</tr>
<tr>
<td></td>
<td>100</td>
<td>32798.9</td>
<td>25980.5</td>
<td>20.78</td>
</tr>
<tr>
<td></td>
<td>150</td>
<td>34660.1</td>
<td>29500.6</td>
<td>14.88</td>
</tr>
<tr>
<td></td>
<td>200</td>
<td>32560.0</td>
<td>28650.5</td>
<td>12.00</td>
</tr>
<tr>
<td>POT-co-NS1</td>
<td>50</td>
<td>33462.0</td>
<td>25541.8</td>
<td>23.66</td>
</tr>
<tr>
<td></td>
<td>100</td>
<td>32560.5</td>
<td>28335.2</td>
<td>12.97</td>
</tr>
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<td></td>
<td>150</td>
<td>32930.0</td>
<td>29926.5</td>
<td>9.12</td>
</tr>
<tr>
<td></td>
<td>200</td>
<td>33100.5</td>
<td>32202.0</td>
<td>2.71</td>
</tr>
</tbody>
</table>

5.4 Role of POT-co-ANS based Copolymer as Corrosion Inhibitor

It was found that the presence of amino naphthol sulphonic acid as a comonomer showed remarkable influence on the anticorrosive performance of the iron. The corrosion inhibition performance of iron increases with increasing the concentration of POT-co-ANS2 inhibitor from 50 to 200 ppm. Weight loss exhibited by iron samples in absence of inhibitor was 40 %. Iron samples showed the minimum weight loss i.e. 2.71 % in presence of inhibitor (POT-co-ANS2) at 200 ppm concentration of.
The corrosion inhibition efficiency of the conducting copolymers of OT and ANS mainly depends on the π-electron conjugation, molecular size, quaternary nitrogen atom and their solubility. Use of polyaniline for corrosion inhibition of iron in acidic medium is restricted due to its insolubility in common organic solvents like methanol and ethanol. To overcome this problem, the copolymers of substituted aniline such as o-toluidine based inhibitor were selected for protection of iron in corrosive medium. Corrosion inhibition of iron in acidic environment by copolymer can be explained on the basis of molecular adsorption. The electrochemical impedance studies showed that these copolymers protect the iron from corrosion in aggressive medium through adsorption mechanism. Availability of lone pair of electrons on the hetero atoms present in comonomer units support the copolymers to exhibit effective corrosion inhibition and greater coverage on the metal surface in acidic medium. Moreover, different functional groups present in naphthylamine ring such as – NH₂, –OH and –SO₃H also responsible for enhancing the corrosion inhibition performance of iron in acidic medium. In acidic solution, amines act as a cation and adsorb onto metal surface through electrostatic interaction between the positively charged anilinium cations hence adsorbed chloride ions [22]. Copolymer consists of OT and ANS act as a protonated species in acidic media which adsorb onto the surface of the iron to form a monomolecular barrier. As with barrier coatings, the adsorbed molecules restrict the anodic or cathodic corrosion reaction by reducing the corrosion rate [22-24]. Presences of delocalized pi electrons on the copolymer chain form co-ordination type of bonds with the iron surface. Iron in acidic medium is negatively charged, the existence of quaternary ammonium nitrogen acts as an anchoring unit which makes the polymer chain attached to the surface. Furthermore, it is also presumed that the bulkiness of substitution in aromatic ring build a cluster network on iron surface anchored more strongly resulting in good coverage of surface and enhanced inhibition efficiency. Solubility of the copolymers in alcohol also play an important role to improve the corrosion inhibition efficiency of iron. Therefore copolymers based on OT and ANSA can effectively be employed as a efficient corrosion inhibitors. Better corrosion inhibition performance shown by POT-co-ANS2 as compared to POT-co-ANS1 is due to the higher concentration of ANS moieties in copolymer chain.

6. CONCLUSION

Highly soluble conducting copolymers based on o-toluidine and 2-amino-5-naphthol-7-sulphonic acid have been synthesized by chemical oxidative copolymerization method. Synthesized copolymers were characterized by FTIR, TGA and SEM characterization to evaluate the structural, thermal and morphological behavior. Tafel polarization studies, electrochemical impedance measurements and weight loss study were carried out to evaluate the inhibition efficiencies of the copolymers at different concentration. Corrosion inhibition efficiency of copolymers increased with increasing inhibitor concentration as well as the incorporation of higher concentration of ANS in copolymer matrix. Impedance measurement gives the Nyquist plot of iron in 1.0 M HCl with and without addition of copolymers from where corrosion kinetic parameters were derived. Corrosion inhibition efficiency was found to be 82 % in case copolymer (POT-co-ANS1) which was increased up to 95 % by using the copolymer (POT-co-ANS2) at 200 ppm concentration. The electrochemical impedance of iron in acidic medium with addition of these inhibitors revealed that these copolymers reduce the rate of corrosion of iron metal through adsorption mechanism. These studies clearly reveal that the synthesized copolymer with higher concentration of ANS unit has excellent corrosion inhibition properties and it can be considered as a potential material for protection of iron in corrosive medium like 1.0 M HCl at low concentration.

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