

“ANALYSIS OF RC FRAMED STRUCTURES WITH CENTRAL AND PARTIAL OPENINGS IN MASONRY INFILL WALL USING DIAGONAL STRUT METHOD”

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Abstract

In Reinforced concrete frames the masonry infill walls are a common practice in countries like India, where the region is prone to seismic activity. In general, the masonry infill walls are treated as nonstructural element in structural analysis and only the contribution of its mass for is considered and it's structural parameters like strength and stiffness is generally ignored in practice, such an approach may lead to an unsafe design. Infill walls resist lateral loads but because of the openings in the infill wall the resistance may slightly reduce. The IS code provisions do not provide guidelines for the analysis and design of RC frames with infill wall and for different percentage of openings. In this study, an office or residential building outer side central opening or outer side partial openings are used and analysis is carried for Bare Frame model, infill walls without opening, infill walls with outer periphery central opening and infill wall with outer periphery partial opening models. In ETABS software G+14 RC framed building models has been prepared, Equivalent Static Lateral force method, Response spectrum method has been performed for analysis as per IS 1893 : 2002 including p-delta effects. Storey displacement, Storey shear, Storey drift, with soft storey considering the effects of infill wall with central and partial openings are the parameters considered in this study. For modeling, the Equivalent diagonal strut method has been used to find out the width of Strut using FEMA 273 .The results for bare frame, infill wall, and infill wall with central and partial openings are discussed and conclusions are made.

Keywords: Equivalent diagonal strut, stiffness, Drift limitation.

1. INTRODUCTION

Earthquake is responsible for the ground motion in all directions, inducing the inertial forces on the structures. Thus the structure has to withstand lateral loads due to earthquake, wind loads along with the gravity loads. Nowadays RC frames are the common construction practice. The gap created between the columns, beams are filled by infill materials like bricks. Due to functional requirements the openings are provided in wall for windows, doors etc.,

In RC buildings the gravity loads do not cause effect, but the lateral loads like wind, earthquake tremors are a matter of great concern and need special design consideration. These lateral loads create critical stress in a building, causing lateral sway and can reach a stage of causing discomfort for the occupants.

The presence of infill walls increases the lateral stiffness, strength and reduces the fundamental period. The presence of openings in the infill walls can reduce some amount in the increase of lateral stiffness due to infill wall.

The behavior of the infill walls subjected to the lateral loads is represented as shown in fig 1. When the lateral loads are applied the infill walls resists to some extent creating gaps at the corners as shown.

If the openings provided in the infill walls are small, its effect may be negligible in stiffness calculation. If the openings are large, it may interfere the diagonal bracing action (fig 2), thereby causing premature shear failure.

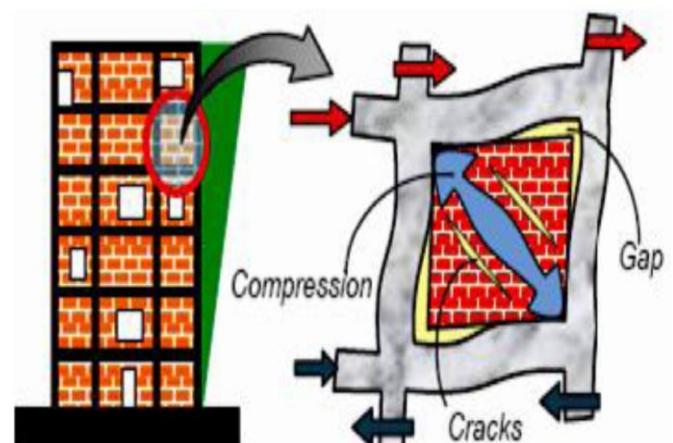


Fig -1: Behavior of the infill wall as a strut member.

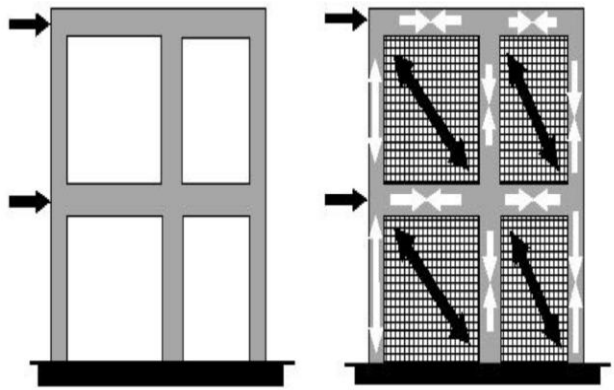


Fig -2: Bracing action of the infill wall

1.1 Types of Infill Provisions

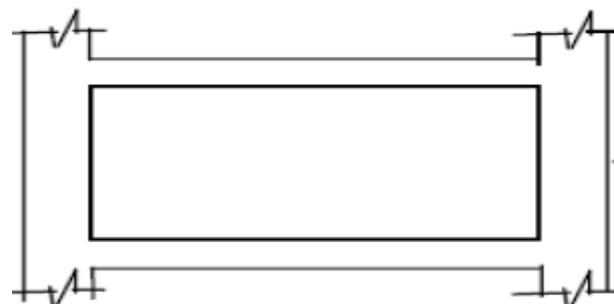


Fig -3: Bare frame

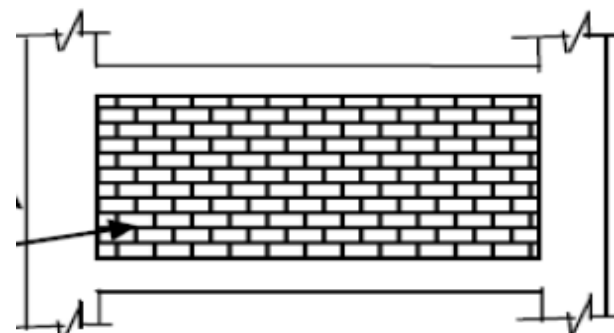


Fig -4: Fully infilled frame

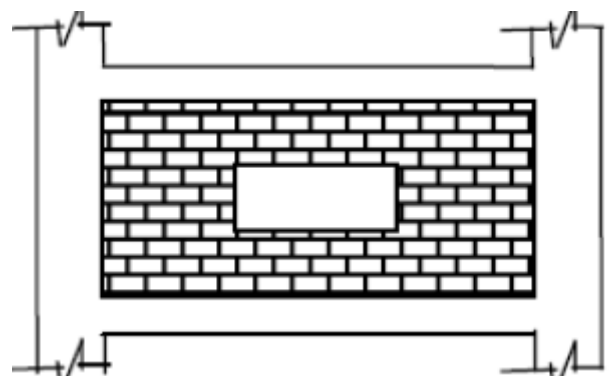


Fig -5: Infilled frame with central opening

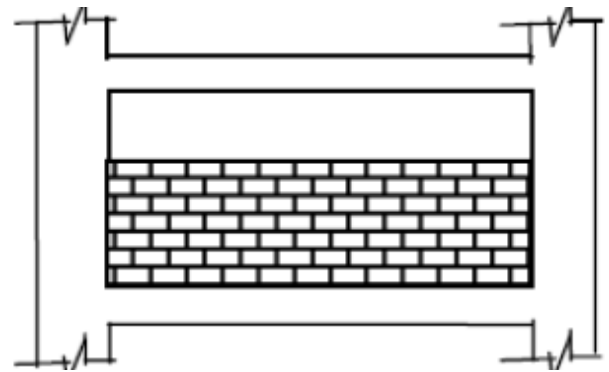


Fig -6: Partially infilled frame

The infill walls are provided in different manner as shown in Fig 3, 4, 5, 6.

2. LITERATURE REVIEW

Many Researchers have developed equations for calculating the “Equivalent Diagonal Strut width”. Some of the major are:

1. In 1961 Holmes,

$$W = \frac{dz}{3} \text{ where, } dz = \text{Diagonal length of infill panel}$$

2. In 1962 Smith,

$$W = \sqrt{\alpha_H^2 + \alpha_L^2}$$

$$\frac{\alpha_h}{L'} = \frac{\pi}{2} \cdot \frac{1}{\lambda_h L'}$$

$$\lambda_h L' = L' \sqrt{\frac{E_{panel} \cdot t \sin 2\theta}{4 \cdot E_p I_p \cdot h}}$$

$$\frac{\alpha_L}{L'} = \pi \cdot \frac{1}{\lambda_L L'}$$

$$\lambda_L L' = L' \sqrt{\frac{E_{panel} \cdot t \sin 2\theta}{4 \cdot E_p I_b \cdot L}}$$

3. In 1969 Smith and Carter,

$$W = 0.58 \left(\frac{1}{H} \right)^{-0.445} (\lambda_h H)^{0.335 dz(x)}$$

where $x = \left(\frac{1}{H} \right)^{0.064}$

$$\lambda_h = \sqrt[4]{\frac{E_s t \sin 2\theta}{4E_c I_h}}$$

4. In 1971 Mainstone,

$$W = 0.175dz (\lambda_h H)^{-0.4}$$

5. In 1984 Liaw and Kwan,

$$W = \frac{(0.95H \cos \theta)}{\sqrt{\lambda_h H}}$$

6. In 1992 Paulay and Priestley,

$$W = \frac{dz}{4}$$

7. In 2009 Chethan.K,

$$W = 1.414\alpha_h,$$

$$\alpha_h = \frac{\pi}{2\lambda} \quad \lambda = \sqrt[4]{\frac{E_m t \sin 2\theta}{4E_c I_h}}$$

3. METHOD OF ANALYSIS OF THE INFILL WALL

3.1 Data Taken

Storey	G+14 (6X4 BAYS)
Typical storey height	3.5m
Beam size	400 X 500 mm
Column size	600 X 600 mm
Live load	3.5 KN/m ²
Floor finish	0.6 KN/m ²
Water proof on terrace load	1.5 KN/m ²
Response reduction factor	5
Type of soil	Medium
Damping factor	5%
Grade of concrete	M30
Steel	Fe500
Density of concrete	25 KN/m ³
Density of brick infill	20 KN/m ³
Poisson's ratio of concrete	0.2
Poisson's ratio of brick infill	0.15
Modulus of elasticity of concrete	22360.67 KN/m ²
Modulus of elasticity of brick infill	4000 KN/m ²
Thickness of slab	150 mm
Thickness of wall	230 mm
Seismic zone	V
Wind speed	50 m/s
Terrain category	2
Structure class	C

3.2 Types of Model

ID	Description
BFGSS0%	Bare frame with ground soft storey without opening.
BFGSS30%	Bare frame with ground soft storey with 30% opening.
BFGSS60%	Bare frame with ground soft storey with 60% opening.
SFGSSC0%	Strut frame with ground soft storey without opening.
SFGSSC30%	Strut frame with ground soft storey with 30% central opening.
SFGSSC60%	Strut frame with ground soft storey with 60% central opening.
SFGSSP30%	Strut frame with ground soft storey with 30% partial opening.
SFGSSP60%	Strut frame with ground soft storey with 60% partial opening.

3.3 Modeling of Infill Wall

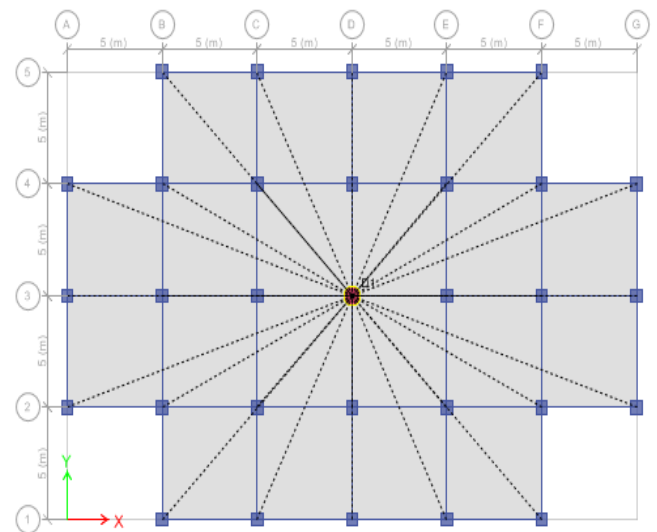


Fig -6: Plan view of the model

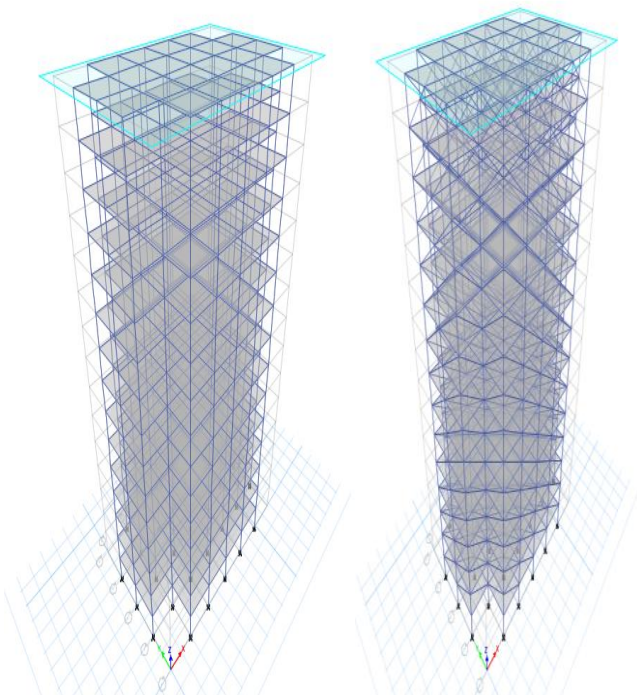


Fig -7: Elevation view of Bare frame and Strut frame

3.4 FEMA Approach

In the case of an infill wall located in a lateral load resisting frame the stiffness and strength contribution of the infill are considered by modeling the infill as an equivalent compression strut. Because of its simplicity, several investigators have recommended the equivalent strut concept. According to FEMA 273, infills are assumed as an equivalent diagonal strut with pin joint at the corners as shown Fig 8.

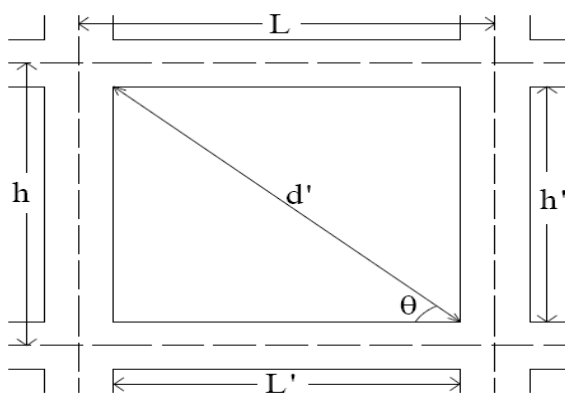


Fig -8: Equivalent diagonal strut for the infill panel

$$W=0.175 [\lambda' h]^{-0.4} d'$$

Where, $\lambda' = \sqrt[4]{(E_i T \sin 2\theta) / (4 E_f I_c H')}$

- T= thickness of wall
- E_i = Elasticity of concrete
- E_f = Elasticity of brick infill

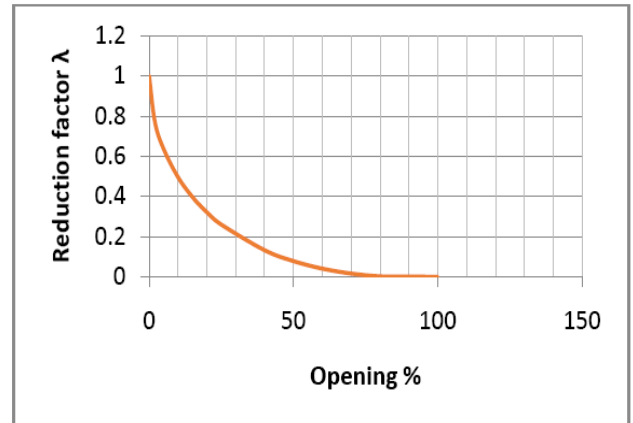


Fig -8: Reduction factor curve

$$\text{Reduction factor} = 1 - 2\alpha_w^{0.54} + \alpha_w^{1.14}$$

$$\text{Opening Percentage (\%)} = \frac{\text{Area of opening (A}_{op}\text{)}}{\text{Area of the infill (A}_{infill}\text{)}}$$

4. RESULT AND DISCUSSION

4.1 Displacement:

Table -1: Displacement in X direction

	EQ	RS	Wind
BFGSS0%	62.5	48.8	30.8
BFGSS30%	59.8	41.7	30.6
BFGSS60%	55.8	38.9	30.6
SFGSSC0%	32.4	23.9	7.4
SFGSSC30%	34.6	24.9	8.7
SFGSSC60%	35.5	25.5	9.1
SFGSSP30%	33.4	24.2	7.9
SFGSSP60%	32.8	24.6	8.4

Table -2: Displacement in Y direction

	EQ	RS	Wind
BFGSS0%	66.3	51.3	50.8
BFGSS30%	63.4	44.2	50.8
BFGSS60%	59.1	41	50.8
SFGSSC0%	37.6	27.7	13.8
SFGSSC30%	37.9	27.9	14.6
SFGSSC60%	38	28.3	14.8
SFGSSP30%	37.8	27.8	13.9
SFGSSP60%	37.9	27.9	14.2

The displacements values for different models as shown in table 1 and table 2. The displacement is reduced by 51% from the bare frame model to the infilled frame model. But when we consider the infilled frame with central opening and partial opening 40 – 45 % of the displacement is reduced.

4.2 Storey Drift:

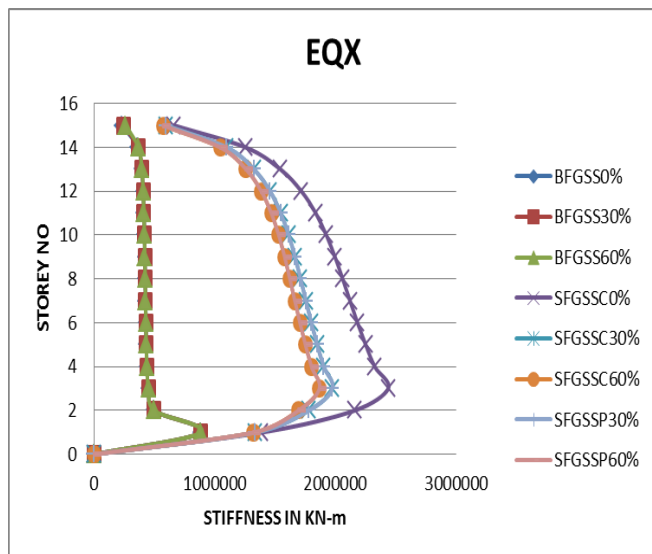


Chart -1: storey drift in X direction

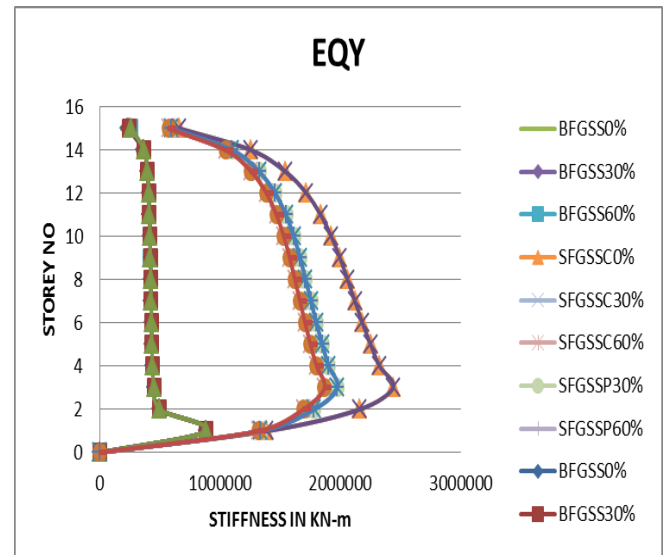


Chart -4: storey drift in Y direction

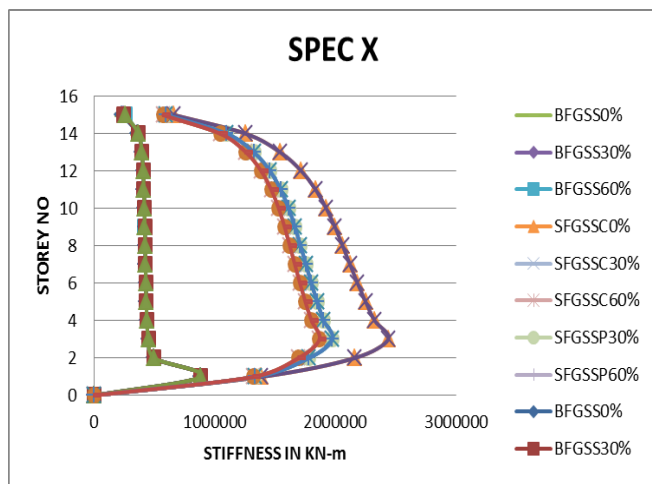


Chart -2: storey drift in X direction

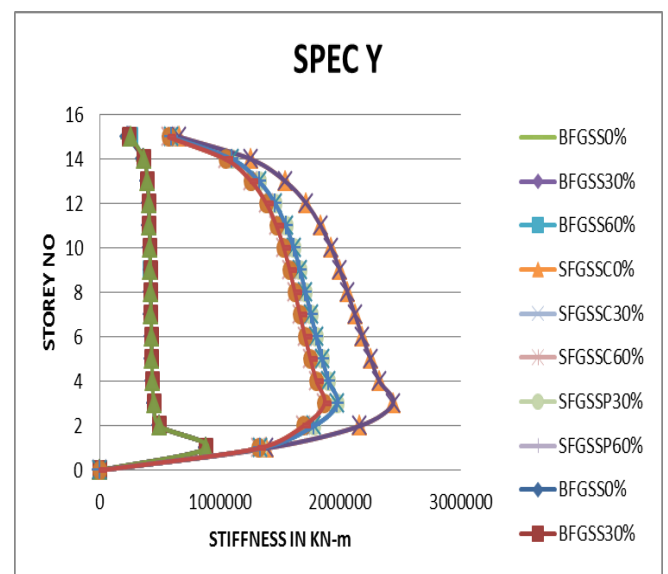


Chart -5: storey drift in Y direction

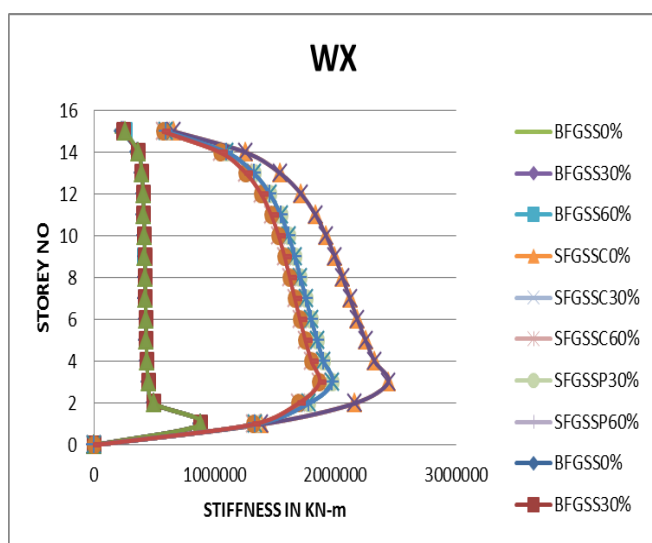


Chart -3: storey drift in X direction

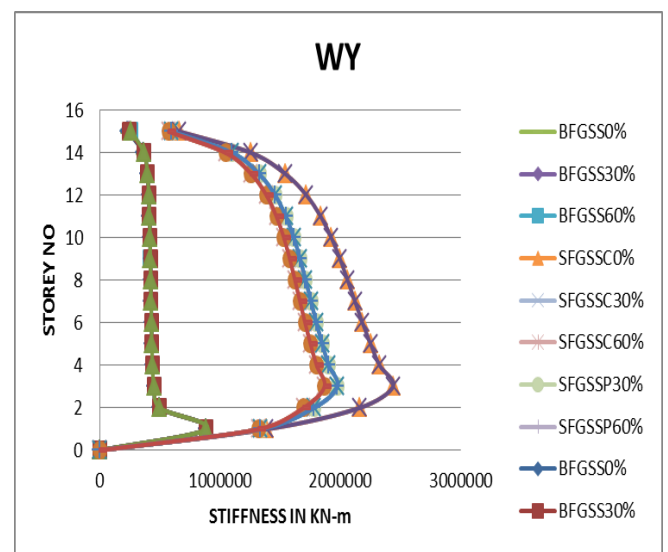


Chart -6: storey drift in Y direction

The storey drift versus storey no is plotted for Equivalent static method , response spectrum method. wind analysis as shown in chart 1 to chart 6. The storey drift for the first storey is higher because of the open ground storey. The drift are within the limitation specified in IS 1893:2002.(ie. 0.004 times storey height)

4.3 Stiffness:

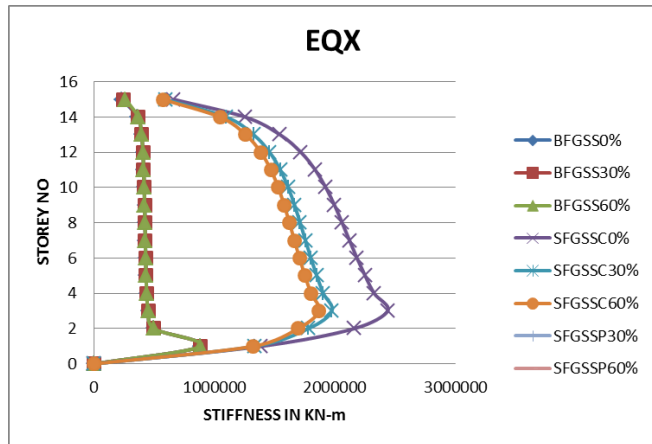


Chart -7: Stiffness in X direction

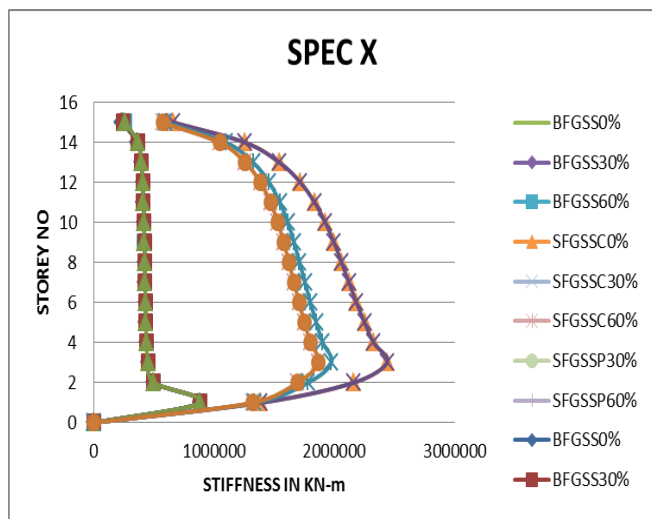


Chart -8: Stiffness in X direction

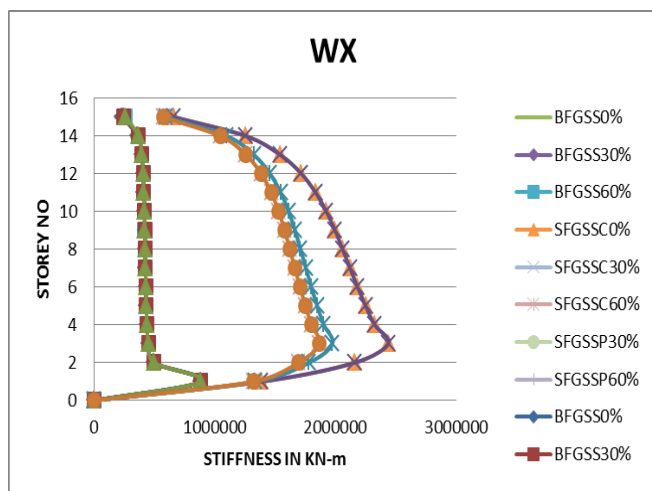


Chart -9: Stiffness in X direction

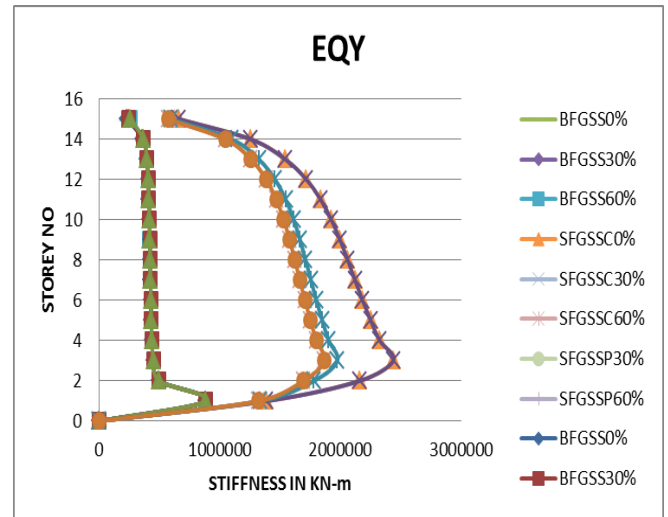


Chart -10: Stiffness in X direction

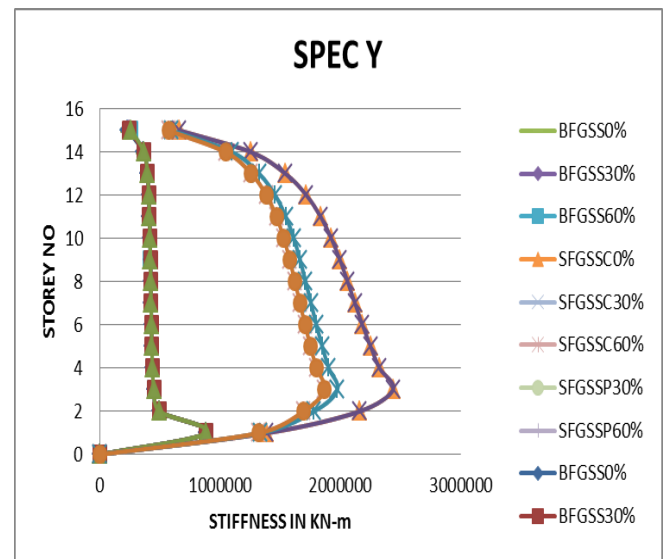


Chart -11: Stiffness in Y direction

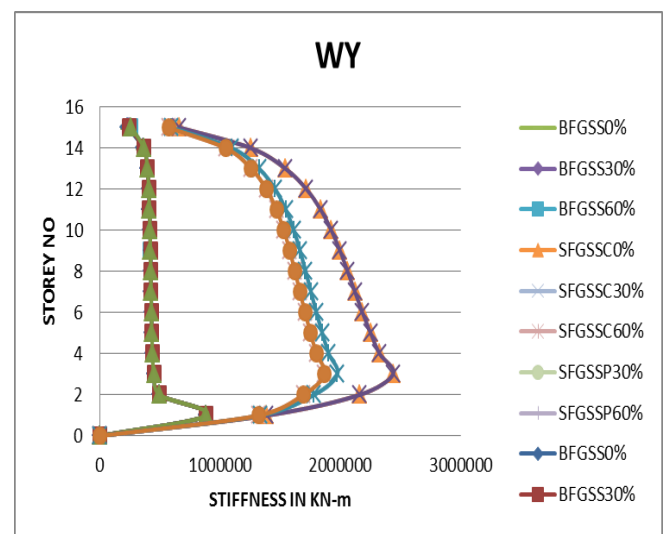


Chart -12: Stiffness in Y direction

The stiffness for different models as shown in Chart 7 to Chart 12. The stiffness is increased by 68 % by considering the effect of infill walls and about 10% reduction due to the opening has been observed.

4.4 Time Period:

Table -3: Time period

mode no	BFGSS0%	BFGSS30%	BFGSS60%	SFGSSC0%	SFGSSC30%	SFGSSC60%
1	2.852	2.73	2.55	1.537	1.572	1.606
2	2.725	2.608	2.436	1.408	1.514	1.582
3	2.492	2.381	2.217	1.25	1.491	1.539
4	0.927	0.887	0.829	0.504	0.516	0.531
5	0.889	0.851	0.795	0.467	0.5	0.52
6	0.815	0.779	0.726	0.414	0.496	0.51
7	0.527	0.504	0.471	0.272	0.29	0.308
8	0.511	0.489	0.457	0.26	0.283	0.288
9	0.472	0.451	0.42	0.243	0.28	0.284
10	0.359	0.344	0.322	0.19	0.205	0.216
11	0.349	0.335	0.313	0.182	0.198	0.202
12	0.323	0.309	0.288	0.172	0.196	0.198
13	0.265	0.254	0.237	0.145	0.157	0.165
14	0.259	0.248	0.232	0.139	0.151	0.155
15	0.239	0.229	0.213	0.132	0.15	0.151

The time period for different models is as shown in table 3. The time period is found to be decreased by 46% from bare frame model to infilled frame model. Because of the presence of the opening the time period has slightly increased compared to infilled frame model.

5. CONCLUSION

In this paper bare frame , infilled frame models with and without opening are prepared for linear static analysis and response spectrum analysis. The p-delta effect also been analysed but the result showed a negligible amount of variations, in that time period has significant changes. From this analysis, it shows that p-delta effect can be considered for higher storey buildings. The displacement values shows that there is a significant decrease in displacement by considering the effect of infills and slight increase in displacement due to openings.

The stiffness is increased by about 70% by considering the effect of infills. The base shear was also found to be increased. It can also be concluded that, the increase in percentage of opening leads to decrease in the lateral stiffness.

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BIOGRAPHIES



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