

STATISTICAL OPTIMIZATION OF ADSORPTION VARIABLES FOR BIOSORPTION OF CHROMIUM (VI) USING CRUDE TAMARIND POD SHELL AND ACTIVATED CARBON

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Abstract

Hexavalent Chromium is a major pollutant released during several industrial operations. In this study low-cost agro waste biosorbent tamarind (*Tamarindus indica*) pod shells with partial and complete Pyrolysed forms were explored for the removal of hexavalent chromium ions from aqueous solution. All the biosorption experiments were carried out in batch mode to optimize process parameters using response surface methodology. Based on central composite design, quadratic model was developed to correlate the variables to the response. Statistical analysis was carried out to identify the most influential factor for all the adsorbents. Through analysis of variance (ANOVA) it was observed that pH is significant for crude and temperature is significant for pyrolysed adsorbent. Among all the adsorbents tested, crude tamarind, removed a maximum of 96.09% of chromium with biomass loading of 4.59g/ 100ml at the optimized conditions of initial concentration 71.7213 mg/l, pH 2.47, and temperature of 41.82°C.

Keywords: Biosorption, *Tamarindus indica*, Hexavalent chromium, Pyrolysis, ANOVA

1. INTRODUCTION

In aqueous system chromium exists in two oxidation states trivalent chromium [Cr (III)]. and hexavalent chromium [Cr (VI)]. Both oxidation states of chromium have different chemical, biological and environmental characteristics [1]. Cr (III) is relatively insoluble and required by microorganisms in small quantities as an essential trace metal nutrient [2], while Chromium [Cr (VI)]. is a great concern because of its toxicity. Chromium (in this text hereafter chromium refers to Cr (VI)) has been reported to be a primary contaminant to humans, animals, plants and microorganisms and it is known to be carcinogenic [3–5].

Chromium is used in a variety of industrial applications hence, large quantities of chromium is discharged into the water bodies. Water bodies and ground water are polluted by chromium by the waste coming out of electroplating fabrication, paints and pigments, mining, leather tanning, etc. [6-8]. Due to environmental concern, discharge limits of chromium have been closely monitored by most industrial countries. Chromium concentration in industrial waste water ranges from 0.5 to 270 mg/l [7]. The tolerance limit for chromium for discharge into inland surface waters is 0.1 mg/l and in potable water is 0.05 mg/l [9, 10]. In order to comply with this limit, it is essential that industries treat their effluents to reduce the chromium concentration in water and wastewater to acceptable levels before its transport and cycling into the natural environment.

Appropriate technologies are applied to reduce the level of chromium in final effluents. In wastewater treatment, various methods utilized to remove chromium include reduction followed by chemical precipitation [11], ion exchange [12], electrochemical precipitation [13], reduction [14], adsorption [15], solvent extraction [16], membrane separation [17], concentration [18], evaporation and reverse osmosis [19, 20].

Above all adsorption is by far most versatile and effective method for removing any contaminants like heavy metal, especially, if combined with appropriate regeneration steps. This solves the problem of sludge disposal and renders the system more economically viable, especially if low cost adsorbents are used [21]. In the last few years, several approaches have been reported in this direction utilizing inexpensive and effective adsorbent for removal of chromium from aqueous solutions. Many biosorbent were tried for chromium removal as seen in literature [22-37]. The materials tried for this purpose range from industrial wastes to agricultural waste products and biomass. Some examples are hydrous concrete particles[22], paper mill sludge [16], seaweed biosorbent [23], sugar beet pulp[24], wheat bran [25], activated groundnut husk carbon[26], coconut husk and palm pressed fibers [27], coconut shell, wood and dust coal activated carbons [28], coconut tree sawdust carbon [29], used tyres carbon [30], cactus, wool, charcoal, and pine needles [31], rice husk carbon [32], hazelnut shell carbon [33,34], almond shell carbon [35], corncob [36]. and cow dung carbon[37].

Agro waste such as tamarind pod shell as biosorbent is promising because of low cost, abundance in availability in India and reasonably high efficiency. It will not be used for any other purpose other than as low grade fuel. In this study tamarind pod shell, partially pyrolysed tamarind pod shell and completely pyrolysed tamarind pod shell were used for chromium removal.

Response Surface Methodology (RSM) is a collection of statistical technique for design of experiments, model building, evaluation of the effects of parameters and optimizing the parameters for maximum removal efficiency. It is widely used for multivariable studies in many processes [38-40]. No work has been carried out with partial and complete pyrolysis of tamarind pod shell. The objective of present study is to quantify the biosorption of chromium by various forms of tamarind pod shell and to select the best out of them. Further, to optimize the process parameters for maximum uptake of chromium using RSM.

2. MATERIALS AND METHODS

2.1 Preparation of Biosorbent

2.1.1 Collection of Tamarind Pod Shells

Natural agro waste biosorbent *Tamarindus indica* pod shells collected from Kolar district, Karnataka were used for removal of chromium. Natural biosorbent along with various pyrolysis processes were employed for comparative metal removal efficiency.

2.1.2 Crude (Untreated) Tamarind Pod Shells (T)

Tamarind pod shells were sun dried, powdered, sieved using 60/80 mesh BSS Standard sieve to get uniform sized particles. The fraction that was retained on 80 mesh were collected, washed thoroughly with distilled water and dried in the hot air oven for 2 hours at 80 °C.

2.1.3 Preparation of Activated Carbon by Pyrolysis

The activated carbons used in this study were prepared by Complete Pyrolysis and Partial Pyrolysis using Crude Tamarind pod shell in a muffle furnace. The complete pyrolysis tamarind (TCP) adsorbent is obtained by just keeping the crucible in the muffle furnace whereas partial pyrolysed tamarind (TPP) is obtained by keeping the lid on the crucible.

2.2 Preparation of Chromium Stock Solution

Synthetic chromium solution was prepared by dissolving potassium dichromate ($K_2Cr_2O_7$) in double distilled water. 1000 ppm of stock chromium solution was prepared by dissolving 2.83 mg of potassium dichromate in one litre of double distilled water. Other required concentrations were prepared by diluting the stock solution. The pH of the solution was adjusted to the required value.

2.2.1 Preparation of Diphenylcarbazide (DPC)

Solution

Diphenylcarbazide (DPC) solution was prepared by dissolving 250mg of DPC in 50ml of acetone in a 100ml volumetric flask.

2.3 Analysis of Chromium

0.25ml of phosphoric acid was added to 1ml of standard sample containing known concentration of chromium, pH was adjusted to 1.0 ± 0.3 using 0.2N sulphuric acid. The solution was mixed well and then diluted to 100ml in a volumetric flask using double distilled water. Further 2ml of DPC solution was added and mixed well. After full colour development for 10min, 4ml of this solution was used in an absorption cell and the concentrations were measured spectrometrically at 540nm in UV-double beam spectrophotometer [Shimadzu- UV Visible 1700]. The calibration curve is prepared by measuring the absorbance of different known concentrations of chromium solutions and plotting a graph between concentrations versus absorbance. A straight line is obtained with R^2 of 0.994.

2.4 Initial Experiments

The initial experiments were conducted to fix limits of the parameters to be varied. Maximum chromium removal is observed with the range of initial metal ion concentrations of 10 – 200 ppm, pH 1-7, temperature 30-50°C and biosorbent dosage of 1 - 10 g/100 ml. These ranges of variables were employed for further study.

2.5 Design of Experiments using Central Composite

Design (CCD) [42]

The parameters initial metal ion concentration, pH, temperature and biosorbent dosage were chosen as independent variables and the removal efficiency of chromium is output response. A 2^4 full factorial experimental design, with seven replicates at the centre point and thus a total of 31 experiments were employed in this study using the statistical software, MINITAB 16 (PA, USA). The centre point replicates were chosen to verify any change in the estimation procedure as a measure of precision property. Each independent variable had 5 levels which were -2, -1, 0, +1 and +2. Therefore, a total of 31 different combinations were chosen in random order according to a CCD configuration for four factors. Table.1 shows the levels of chosen variables used in the experiment for the removal of chromium.

The analysis focused on how the removal efficiency is influenced by independent variables, metal concentration (X_1), pH (X_2), temperature (X_3) and biosorbent dosage (X_4). The dependent output variable is maximum removal efficiency (Y).

2.6 Response Surface Methodology (RSM)

Response surface methodology is an empirical statistical technique employed for multiple regression analysis by using quantitative data obtained from properly designed experiments to solve multivariate equations simultaneously. The experiments with different metal ion concentration, pH, temperature and adsorbent dosage were employed simultaneously covering the spectrum of variables for the removal of chromium in CCD.

Table 1: Central composite design for biosorption of chromium

Independent variable	Range and Level				
	-2	-1	0	+1	+2
(X ₁)	50	87.5	125	162.5	200
(X ₂)	1	2.5	4.0	5.5	7
(X ₃)	30	35	40	45	50
(X ₄)	1	3.25	5.5	7.75	10

Where

(X₁) is Initial Chromium ion concentration (ppm)

(X₂) is pH

(X₃) is Temperature (°C)

(X₄) is Biomass loading (g/100 ml)

The regression analysis was performed to estimate the response function as a second order polynomial as shown in equation 1

$$Y = \beta_0 + \beta_1 X_1 + \beta_2 X_2 + \beta_3 X_3 + \beta_4 X_4 + \beta_{11} X_1^2 + \beta_{22} X_2^2 + \beta_{33} X_3^2 + \beta_{44} X_4^2 + \beta_{12} X_1 X_2 + \beta_{13} X_1 X_3 + \beta_{14} X_1 X_4 + \beta_{23} X_2 X_3 + \beta_{24} X_2 X_4 + \beta_{34} X_3 X_4 \dots \dots \dots (1)$$

X₁, X₂, X₃, X₄ are linear effects, X₁², X₂², X₃², X₄² are squared effects, X₁X₂, X₁X₃, X₁X₄, X₂X₃, X₂X₄, X₃X₄ are interaction effects and Y is the predicted response. β₀ is constant coefficient, β₁, β₂, β₃, β₄ are linear coefficients, β₁₁, β₂₂, β₃₃, β₄₄ are squared coefficients, and β₁₂, β₁₃, β₁₄, β₂₃, β₂₄, β₃₄ are interactive coefficients, respectively.

A statistical software package Minitab 16, was used for regression analysis of the data obtained and to estimate the coefficient of the regression equation. The equations were validated by the statistical test called ANOVA. The significance of each term in the equation is to estimate the goodness of fit in each case. Response surface were drawn to determine the individual, square and interactive effects of test variable on percentage removal of chromium.

2.7 Batch Experiments

Batch adsorption studies were performed by Shaking 100 ml of different solutions in 250 ml conical flasks with cork lid in constant temperature shaker at the conditioned mentioned by central composite design to obtain the equilibrium data.

All experiments were performed in triplicate and the results were averaged. After specified time interval, the samples were analysed by the spectrophotometric method.

2.8 Optimization of Parameters

The second degree polynomial equation is solved and the optimum values for the variables are obtained using response optimizer in Minitab 16.

3. RESULTS AND DISCUSSIONS

3.1 Central Composite Design (CCD) Analysis

The results of experiments performed according to the CCD design are given in Table 2. Table 2 gives the experimental results along with the predicted values (section 3.2) for all three adsorbents T, TCP and TPP.

It may be observed from Table 2 that the percentage removal is higher at lower pH. In acidic pH, the biosorbent surface may be protonated and hence the positively charged biosorbent removes higher amounts of Chromium in the anionic form HCrO₄⁻. With the increase in the pH of the system, the degree of protonation on the surface reduces gradually and hence at higher pH, above 3.0, other mechanism like physical adsorption on the surface of sorbent could have taken an important role in sorbing Chromium and exchange mechanism might have reduced.

Further, the effect of temperature is significant on pyrolysed type of adsorbent suggests that the biosorption between chromium and pyrolysed tamarind adsorbent involve the combination of chemical interaction and physical adsorption. With the increase in temperature the pores in the adsorbent enlarges resulting in getting more surface area available for diffusion and adsorption. [43]

3.2 Response Surface Methodology (RSM)

Regression analysis was done to fit the response function as per the equation 1 and the results are reported as eq.2, eq.3 and eq. 4 for T, TCP, TPP, respectively

$$Y = 92.9229 - 3.3183X_1 - 13.3267X_2 + 5.4933X_3 + 5.6333X_4 - 1.1537X_1^2 - 19.6637X_2^2 + 0.70639X_3^2 - 3.0737X_4^2 + 4.0000X_1X_2 - 0.8400X_1X_3 - 14.2250X_2X_3 + 7.5050X_2X_4 + 3.0650X_3X_4 \dots \dots \dots (2)$$

$$Y = 75.68 - 0.84X_1 - 4.7X_2 + 11.9467X_3 + 2.2983X_4 + 1.0242X_1^2 - 15.4858X_2^2 - 0.2308X_3^2 + 10.9492X_4^2 - 10.825X_1X_2 - 10.19X_1X_3 + 4.3450X_1X_4 + 17.94X_2X_3 - 0.715X_2X_4 + 7.4X_3X_4 \dots \dots \dots (3)$$

$$Y = 70.38 - 1.36X_1 - 4.9883X_2 + 11.7750X_3 + 1.8783X_4 + 1.1200X_1^2 - 14.5850X_2^2 - 0.4850X_3^2 + 10.8500X_4^2 - 10.3600X_1X_2 - 7.5600X_1X_3 + 5.5650X_1X_4 + 16.78X_2X_3 + 0.2950X_2X_4 + 8.9550X_3X_4 \dots \dots \dots (4)$$

These above equations explain the effect of individual variable (linear and squared) and interactive effects on Chromium adsorption onto different adsorbent. The chromium removal was predicted using eq.2 – eq.4 at experimental parameters and the obtained values are also reported in Table 2.

Multiple regression coefficient R^2 is calculated from the second degree polynomial equation (equation 2,3 and 4), is $R^2= 0.8612$ for T, 0.7995 for TCP and 0.7561 for TPP indicates that the predicted values are closer to experimental data as shown in Table 2. For a good statistical model, R^2 value should be closer to 1, and a value of 0.75 indicates aptness of the model. The R^2 value of 0.8612 for T implies

that more than 86.12% of experimental data was compatible with the model and only less than 13.88% of the variations are not explained by the model [44].

The experimental results were analysed and student 't' test was conducted to find the significance of individual parameters, squared parameters and interactive parameters combination, smaller the probability value more significant is the effect. The regression coefficients, 't' test results and probability values are reported in Table 3. The results show that pH and square effect of pH is significant for crude tamarind (probability value, $p=0.000$) whereas temperature becomes significant for complete and partial pyrolysed tamarind.

Table 2. Central Composite Design Matrix of design specifications along with observed response for chromium removal by T, TCP & TPP

Run Order	Concentration	pH	Temperature	Biomass loading	% Chromium removal					
					T		TCP		TPP	
					Theoretical	Experimental	Theoretical	Experimental	Theoretical	Experimental
1	125	4	40	5.5	89.32	88.67	75.68	70.18	70.38	68.83
2	87.5	5.5	35	3.25	69.68	66.88	70.62	65.74	67.53	65.87
3	162.5	2.5	45	7.75	92.19	94.34	86.8	81.12	82.09	78.43
4	162.5	2.5	45	3.25	83.59	85.43	89.21	85.48	84.77	86.27
5	50	4	40	5.5	91.85	88.89	71.18	67.89	66.68	67.23
6	87.5	2.5	45	3.25	89.70	92.34	86.78	79.15	81.23	76.78
7	162.5	5.5	45	7.75	90.36	90.90	78.39	72.23	73.4	70.23
8	87.5	2.5	35	3.25	88.98	87.78	83.36	77.36	81.02	75.67
9	162.5	2.5	35	3.25	89.51	88.11	84.59	80.55	79.08	77.87
10	87.5	5.5	35	7.75	85.74	86.01	53.68	52.45	48.71	50.23
11	125	4	40	10	90.60	89.14	90.83	86.89	85.23	81.43
12	87.5	5.5	45	7.75	89.21	87.45	89.91	91.23	89.61	86.56
13	125	4	40	5.5	89.44	90.88	75.68	77.03	70.38	72.34
14	125	4	30	5.5	90.36	91.45	56.58	53.28	50.75	51.11
15	87.5	2.5	35	7.75	87.93	88.56	72.2	75.35	66.32	64.34
16	125	4	40	1	83.34	82.17	63.79	66.56	58.57	56.72
17	125	4	40	5.5	88.34	86.36	75.68	71.72	70.38	67.66
18	125	4	40	5.5	90.34	89.90	75.68	79.58	70.38	72.45
19	200	4	40	5.5	82.93	83.49	63.59	60.14	57.66	57.78
20	162.5	5.5	35	7.75	81.45	80.79	61.89	63.33	56.93	54.21
21	125	1	40	5.5	97.08	97.27	44.56	46.80	40.4	43.45
22	87.5	2.5	45	7.75	94.93	96.90	83.59	80.90	78.75	74.56
23	125	4	40	5.5	89.34	88.15	75.68	73.51	70.38	67.67
24	125	4	40	5.5	88.34	87.89	75.68	74.72	70.38	67.56
25	125	4	50	5.5	90.14	89.18	75.68	73.35	70.38	65.79
26	125	7	40	5.5	45.68	47.79	57.19	58.11	52.53	55.65
27	162.5	2.5	35	7.75	89.26	91.90	89.53	84.93	82.96	78.89
28	162.5	5.5	35	3.25	71.80	73.76	66.78	68.84	60.59	58.75
29	162.5	5.5	45	3.25	88.38	87.68	80.59	77.57	75.2	73.21
30	125	4	40	5.5	87.34	88.68	75.68	73.57	70.38	66.74
31	87.5	5.5	45	3.25	86.35	84.48	86.55	84.46	80.13	79.12

3.3 Analysis of Variance (ANOVA)

The results of multiple linear regressions conducted for the second order response surface model by ANOVA are given in Table 4. The Fischer's variance ratio, F value = (S_r^2/S_e^2) , is the ratio of mean square owing to regression to the mean square owing to the error. The higher the F -value and lower

the probability P value (< 0.01) demonstrates significance for the regression model. From Table 4 it is seen that linear effect was significant in all cases and square effect is also significant in the case of Crude tamarind

Table 3. Student "t" test analysis for bio sorption of chromium by T, TCP & TPP

Term	Regression Coefficient			t			P		
	T	TCP	TPP	T	TCP	TPP	T	TCP	TPP
Constant	92.9229	75.6800	70.38	35.12	17.877	16.817	0.000	0.000	0.000
Concentration	-3.3183	-0.8400	-1.36	-1.161	-0.184	-0.172	0.263	0.857	0.809
pH	-13.3267	-4.7000	-4.988	-4.664	-1.028	-1.003	0.000	0.319	0.287
Temperature	5.4933	11.9467	11.775	1.922	2.613	2.243	0.073	0.019	0.012
Biomass loading	5.6333	2.2983	1.878	1.971	0.503	0.479	0.066	0.622	0.601
Concentration*Concentration	-1.1537	1.0242	1.120	-0.220	0.122	0.106	0.828	0.904	0.839
pH*pH	-19.6637	-15.4858	-14.585	-3.756	-1.848	-1.583	0.002	0.083	0.074
Temperature*Temperature	0.7063	-0.2308	-0.485	0.135	-0.028	-0.016	0.894	0.078	0.069
Biomass loading*Biomass loading	-3.0737	10.9492	10.850	-0.587	1.307	1.156	0.565	0.210	0.182
Concentration*pH	4.0000	-10.8250	10.360	0.571	-0.966	-0.856	0.576	0.348	0.313
Concentration*Temperature	-0.8400	-10.1900	-7.560	-0.120	-0.910	-0.789	0.906	0.376	0.324
Concentration*Biomass loading	-1.2800	4.3450	5.565	-0.183	0.388	0.318	0.857	0.703	0.678
pH*Temperature	14.2250	17.9400	16.78	2.032	1.602	1.497	0.059	0.129	0.111
pH*Biomass loading	7.5050	-0.7150	0.295	1.072	-0.064	-0.057	0.300	0.950	0.889
Temperature*Biomass loading	3.0650	7.4000	8.955	0.438	0.661	0.564	0.667	0.518	0.473

Table 4. Analysis of Variance (ANOVA) for the selected quadratic model for the removal of Chromium by T, TCP & TPP

Source	DF			Sum of squares			F			Prob>F		
	T	TCP	TPP	T	TCP	TPP	T	TCP	TPP	T	TCP	TPP
Regression	14	14	14	2498.73	2361.15	2359.62	3.64	1.34	1.32	0.008	0.283	0.276
Linear	4	4	4	1503.14	1024.80	1020.37	7.67	2.04	2.01	0.001	0.13	0.11
Square	4	4	4	709.18	719.33	715.56	3.62	1.43	1.38	0.028	0.268	0.259
Interaction	6	6	6	286.41	617.01	612.96	0.97	0.82	0.80	0.473	0.571	0.566
Residual Error	16	16	16	783.91	2007.27	2006.18						
Total	30	30	30	3282.64	4368.42	4364.44						

3.4 Optimization of Response

The optimization of process variables are done to get maximum % removal using response optimizer in Minitab 16. In this regard second degree polynomial equations (eq.2, eq.3 and eq.4) were used to get the optimum values for the variables. Table 5 gives the optimum values for all adsorbents. Maximum removal of 96.09% chromium was achieved with crude tamarind at initial concentration

(71.7213 mg/l), with least biomass (4.59g/ 100ml) and at lower temperature (41.82°C) in acidic medium (pH 2.47).

Table 5. Optimized parameters for T, TCP and TPP

Biosorbent	Initial metal ion Concentration (ppm)	pH	Temperature (°C)	Biomass Load (g/l)	Predicted % Chromium Removal	Experimental % Chromium Removal
T	71.7213	2.47	41.82	4.59	96.86	96.09
TCP	79.9180	2.961	48.56	9.0246	91.08	90.36
TPP	95.0350	2.259	48.8364	9.8701	88.19	86.56

4. CONCLUSIONS

In the present work biosorption of chromium was studied in batch experiments using three types of biosorbent derived from tamarind fruit shell. Central composite design was adopted to study of effect of variation in parameters like initial chromium concentration, pH, temperature and adsorbent dosage. For all the adsorbents, it is observed from the student “t” test that for non- pyrolysed type of adsorbents, pH was significant and the temperature becomes significant for pyrolysed samples. ANOVA analysis reveals that for all the adsorbents linear effect was significant and for crude tamarind square effect is also significant. Analysis of variance also showed that a reasonably high regression coefficient of 0.8612, ensuring a satisfactory adjustment of the second order regression model with the experimental data.

The optimization of process variables indicates that crude tamarind removed maximum chromium of 96.09% with initial metal concentration of 71.7213 mg/l, pH of 2.47, temperature of 41.82 °C and lowest biomass loading of 4.59 g/100 ml. The study clearly demonstrating the use of crude tamarind pod shell which is abundant and available at throw away price may be used to treat a chemical waste containing chromium.

5. NOMENCLATURE

T-Tamarind crude

TCP-Tamarind crude completely pyrolysed

TPP- Tamarind crude partially pyrolysed

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