

# ENERGY AND EXERGY ANALYSIS FOR BIOMASS CO-FIRING COAL FUEL BASED THERMAL POWER PLANT

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## Abstract

Environmental pollution and its control has been one of the most challenging problems to the mankind, especially to the scientific and engineering community. Out of the various environmental polluting sources, excess CO<sub>2</sub> in atmosphere is the single largest contributor for global warming effect. This CO<sub>2</sub> imbalance in the atmosphere is caused by excessive release of CO<sub>2</sub> to the environment from various the man-made industries, like power plants, chemical plants, automobiles, etc. Since coal fuel based power plants are concentrated large source of production of excess CO<sub>2</sub>, attention is focused on sequestration of CO<sub>2</sub> to maintain the environmental CO<sub>2</sub> balance. However, due to its cost intensiveness and technological difficulties, implementation of CO<sub>2</sub> sequestration option has not been adopted by all. A detailed exergy analysis of the control volume has been carried out considering physical and chemical exergy of all the streams and presented in this dissertation. It has been concluded from the results of this analysis that biomass co-firing option may only be considered as a short-term measure to reduce the CO<sub>2</sub> production since the exergy losses including the irreversibility losses are more compared to only coal based power plants.

**Keywords:** Energy and exergy analysis, Biomass co-firing, Thermal power plant, Environmental pollution etc.

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## 1. THEORETICAL ANALYSIS

Energy is one of the major inputs for the economic development of any country. In case of the developing countries, the energy sector assumes a critical importance in view of the ever-increasing needs. As the world is becoming more advanced in technology, more energy is being used to keep up with the changing requirements. The world's primary energy resource is the fossil fuel-coal, and if the current rate of utilization of energy is being continued, the world will shortly come to an end of fossil fuel- coal. Hence energy policy is promoting many researches both for the enhancement of utilization of renewable energy and low enthalpy fuels for power generation and for finding the most effective ways of using them.

Coal fired power plants are normally getting the edge over the other possibilities, since coal is abundantly available and the implementation time is relatively short. The major source of energy which is available in India for thermal power plants is coal. In 1947 the total power generation capacity was only 1360MW, and by 1991 it grew to 65000MW, of which 69% (45000MW) was generated in thermal power plants. The total installed power generating capacity in India is about 1, 25,000 MWe with coal-based thermal power plants comprising 55% of the total (Ministry of Power, 2006). The proven global coal reserve was estimated as 984453 million tones at the end of 2003. The USA had the largest share of the global reserve

(25.4%) followed by Russia (15.9%), China (11.6%). India was 4th in the list with 8.6%. India has huge coal reserves, at least 84396 million tones of proven recoverable reserves (at the end of 2003). This amount to almost 8.6% of the world reserves and it may last for about 230 years at the current reserve to production (R/P) ratio. Coal production is concentrated in these states (Andhra Pradesh, Uttar Pradesh, Bihar, Madhya Pradesh, Maharashtra, Orissa, Jharkhand, and West Bengal). According to the present data the present power position in India is approximately 100 GW whereas it is estimated the demand of power will go to 240 GW by the year 2012.

### 1.1 Methodologies for System Analysis

Traditionally, the thermodynamic analysis of any thermal system is carried out with help of the First Law of Thermodynamics. It gives basically the energy utilization scenario of the thermal system in terms of conservation of energy. This kind of analysis, however, is unable to provide information regarding the losses both qualitatively and quantitatively. Moreover it could not locate where these losses actually occur in a system. All these drawbacks are overcome with the application of the exergy concept based on the Second Law of Thermodynamics. The exergy is the maximum amount of theoretical useful work obtainable in bringing the state of the system of interest into state of environment. Thus, exergy is a measure of the departure of the state of a system

from that of the environment. Unlike energy, exergy can never be conserved; rather some of it is destroyed in any real process. Even though exergy concept was developed in the early part of 20th century, the regular use of exergy analysis started in the second half of the century and became the focus of attention for energy conservation in all kinds of energy applications. Exergy was particularly valuable because it allows a uniform basis to compare between disparate processes. That is why, in recent years there has been a growing trend in the using of Second Law of Thermodynamics in analyzing thermal systems. This analysis provides the information about not only the losses of any thermal systems qualitatively as well as quantitatively, but also their location. The information obtained from the exergy analysis can be used for further improvement in the design and operation of thermal systems. With this information, the design engineers are able to find out the components where exergy destructions are more. Then, the component interdependencies are evaluated to study how the system varies with the design changes in the component.

## 1.2 Available Thermodynamic Analysis

### 1.2.1 Energy Analysis

Several thermodynamic approaches are possible to analyze the operational performance of a thermal power plant. The First Law of Thermodynamics based analysis provides the performance of a thermal system based on conservation of energy. The principle of conservation of energy states that energy can neither be created nor be destroyed, although it can be changed from one form to another. Thus in any isolated or closed system, the sum of all forms of energy remains constant. Of particular interest is the special form of the principle known as the principle of conservation of mechanical energy which states that the mechanical energy of any system of bodies connected together in any way is conserved, provided that the system is free of all frictional forces, including internal friction that could rise during collisions of the bodies of the system [1]. However, First Law analysis does not clarify where and why there are performance degradations, which are mainly due to irreversibilities generated in system or process whereas, The Second Law analysis determines the magnitude and direction of irreversible processes in a system and thereby provides an indicator that points the direction in which engineers should concentrate their efforts to improve the performance of the thermal systems.

### 1.2.2 Exergy Analysis

The second law analysis is based on the concept of exergy The term exergy was introduced by Rant in 1953, which is extensively discussed in the books of Kotas and Szargut et al. [13]. A possibility to work exists whenever a system at a given state interacts with another system at a different state, while they are allowed to come into an equilibrium state. Assuming

one of the two systems as environment and the other as system of interest, exergy or availability can be defined as the maximum amount of theoretical useful work obtainable in bringing the state of the system of interest into the state of the environment. Based on this analysis one can find out all the irreversible losses through exergy destruction, thus provides the real picture of the performance of any thermal system. Thus, this tool becomes very important in analyzing any thermal system.

All the work that has been published with biomass co-firing coal-fired power plants shows only the energy analysis and environmental impact of reducing emission of CO<sub>2</sub>, SO<sub>2</sub>, and NO<sub>x</sub>. Therefore the exergy analysis for biomass co-firing coal fuel based power plant is considered in the present work to achieve at the following objectives

- To study the important of biomass co-firing in coal fuel based power plant.
- To study the various co-firing option in coal fuel based power plant.
- To study the exergy analysis of a biomass co-firing in coal fuel based power plant.

According to the given data the coal used in the plant is eastern bituminous coal with 1.9% sulphur, 7.2% moisture, 8.8% ash, and 31751 kJ/kg of Higher Heating Value (HHV). The ultimate analysis of eastern bituminous coal gives the detailed chemical composition of different constituents which are tabulated in Table 1.

## 1.3 Energy and Material Balances

The energy and material balances for baseline coal only and 15% co-firing option has already been done on the plant and given in Table 1 and Table 2, respectively.

## 1.4 Assumptions for Analysis

- 1) The environment is treated as at 27° C .
- 2) The air required for combustion is considered to be 21% oxygen and 79% nitrogen on molar basis and on mass basis it is 23.2% oxygen and 76.8% nitrogen.

**Table 1** Energy Balance of the plant (GJ/hr)

Heat In	Baseline Coal Only	15% Co-fired
Coal	1092.9	940.6
Biomass	---	166.6
Total	1092.9	1106.6
Heat Out		
Net steam turbine output	360.1	360.1
Auxiliary power use	23.0	23.0
Condenser	587.0	587.0
Stack gas loss	97.6	112.1
Boiler radiation losses	3.4	3.4

Unburned carbon loss	5.5	4.4
Unaccounted for boiler heat loss	16.4	16.6
Total	1092.9	1106.6

**Table 2** Material Balance of the plant (Mg/hr)

Mass In	Baseline Only	Coal	15% Co-fired
Coal	37.1	31.9	
Biomass		11.1	
Combustion air	525.3	533.0	
Lime stone	0.0	0.0	
Feed Water Makeup	0.0	0.0	
Total	562.4	576.0	
Mass Out			
Bottom ash	0.7	0.6	
Fly ash	2.8	2.4	
Flue gas	558.9	573.0	
Gypsum	0.0	0.0	
Total	562.4	576.0	

- The air and combustion gases are treated as ideal gas behavior
- The nitrogen present in the combustion air is inert in nature and has no effect in chemical reaction.
- The flue gas is consisting of CO<sub>2</sub>, SO<sub>2</sub>, H<sub>2</sub>O<sub>gas</sub>, O<sub>2</sub>, and N<sub>2</sub>.

**2. RESULTS AND DISCUSSIONS**

**2.1 Operating Plant Data at Various State Point**

The success of any thermodynamic analysis of an existing plant depends upon the accurate operational data. The operational data at various state points with reference to the control volume shown in Figure 1 is tabulated in Table 3.

**Table 3:** Operational Data for the Plant

State Points	Components	Pressure ( Bar )	Temperature ( °C )	Mass(Mg/hr)	
				Coal Only	15% Cofiring
1	Coal In	1.01325	27	37.1	31.9
2	Biomass In	1.01325	27	0	11.1
3	Combustion Air In	1.01325	38	525.3	533
4	Steam Out	165	538	0.842	0.842
5	Flue gas with fly ash	1.01325	129	558.9	573
6	Bottom Out	1.01325	1327	0.7	0.6

**2.2 Calculation of Physical Exergy**

To calculate the physical exergy the properties data such as enthalpy and entropy data of respective state points corresponding to their temperature is first needed. The same is

calculated first and summarized in Table 6.3. In the present work data for properties evaluation is taken from NIST-JANAF Thermochemical Tables and for super heated steam by Moran and Shapiro [1].

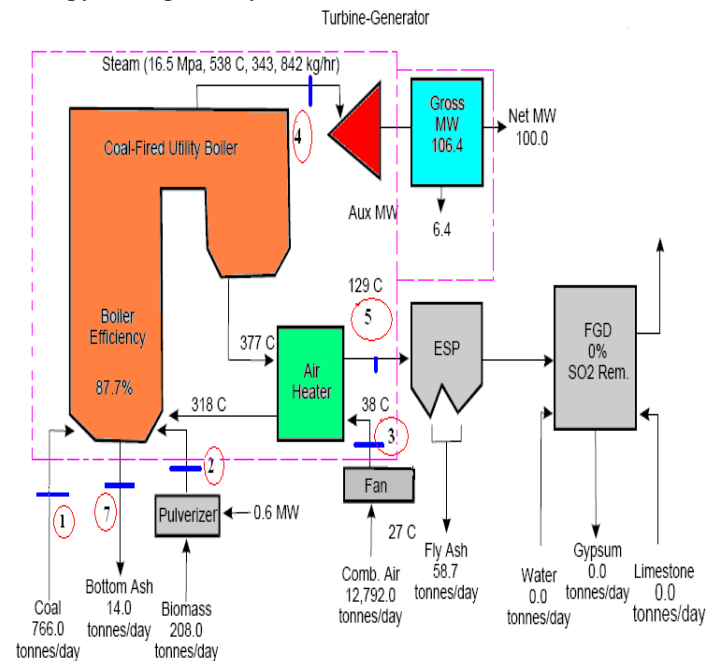
**State Point 1 and 2**

The enthalpy of any fuel is its higher heating value (HHV). The HHV for coal and biomass are shown in Table 1 and 2, respectively.

**State Point 3**

The air considered being ideal gas mixture consisting of 21% oxygen and 79% nitrogen by molar basis. It is entering to the boiler at 38°c = 311.15K .

According to the Eqs. (4.19) and (4.20) the enthalpy and entropy be respectively



**Fig 1** Control Volume for the Plant

$$\bar{h}_3 = 0.21 \times \bar{h}_{O_2} + 0.79 \times \bar{h}_{N_2} = 379.84681 \text{ kJ/kmol}$$

$$\bar{s}_3 = 0.21 \times \bar{s}_{O_2} + 0.79 \times \bar{s}_{N_2} = 199.91028 \text{ kJ/kmol.K}$$

**State Point 4**

At this point the steam is leaving at temperature 538°c and 165bar

From the super heated steam data it is interpolated between 160bar and 180bar and found to be

$$\bar{h}_4 = 3404.778 \text{ kJ/kg} \quad \text{and} \quad \bar{s}_4 = 6.4181 \text{ kJ/kg.K}$$

**State point 5**

The state point 5 is consists of flue gas along with fly ash. The enthalpy of this point is the summation of two. Using chemical formula for coal and biomass from Table 5.3.1 and 5.3.2 respectively and with chemical reaction of Eq. (4.13) the composition of the flue gas is found out and summarized in Table 4.

**Table 4** Composition of Flue Gas

Constituent	kmol/100 kg	
	Coal	Biomass
CO <sub>2</sub>	11.47	11.82
SO <sub>2</sub>	0.12	0.004
H <sub>2</sub> O	5.43	12.5
O <sub>2</sub>	6.76	6.2
N <sub>2</sub>	76.22	69.482

The enthalpy and entropy of flue gas using Eqs (4.19) and (4.20) is

$$\bar{h}_{flue\ gas} = -55513.99363 \text{ kJ/kmol}$$

$$\bar{s}_{flue\ gas} = 207.3768443 \text{ kJ/kmol.K}$$

With the data from Table 5.3.3 we have

$$\bar{h}_{fly\ ash} = -1006576.361 \text{ kJ/kmol.}$$

$$\bar{s}_{fly\ ash} = 94.39433565 \text{ kJ/kmol.K}$$

**State Point 6**

Through state point 6 the bottom ash taken out at temperature 1600 K . Similar to the above procedure and same equation the properties at point 6 is

$$\bar{h}_6 = 0.52 \times \bar{h}_{SiO_2} + 0.21 \times \bar{h}_{Al_2O_3} + 0.0102 \times \bar{h}_{TiO_2} + \dots + 0.0125 \times \bar{h}_{Na_2O} + 0.02 \times \bar{h}_{K_2O}$$

$$= -899294.3887 \text{ kJ/kmol}$$

$$\bar{s}_6 = 0.52 \times \bar{s}_{SiO_2} + 0.21 \times \bar{s}_{Al_2O_3} + 0.0102 \times \bar{s}_{TiO_2} + \dots + 0.0125 \times \bar{s}_{Na_2O} + 0.02 \times \bar{s}_{K_2O}$$

$$= 217.7493 \text{ kJ/kmol.K}$$

**Physical Exergy for Baseline Coal Only**

Using the equations above data the physical exergy at all points are calculated and shown in Table 5 for coal only and in Table 5 for 15% co-firing.

**Table 5** Physical Exergy for Baseline Coal Only

State Points	Enthalpy (kJ/kmol)	Entropy (kJ/kmol.K)	Physical Exergy (GJ/hr)
1	HHV <sup>a</sup>		0
2	HHV <sup>b</sup>		0
3	379.84681	199.91028	0.44262
4	3404.778	6.4181	1.249967
5	-55513.99363 for flue gas and -1006576.361 for fly ash	207.3768443 for flue gas and 94.3943565 for fly ash	231.9763
6	-899294.3887	217.7493	0.580248

<sup>a</sup> – refer to Table 1;

<sup>b</sup> – refer to Table 2

**Table 5** Physical Exergy for 15% Co-firing

State Points	Enthalpy (kJ/kmol)	Entropy (kJ/kmol.K)	Physical Exergy (GJ/hr)
1	HHV <sup>a</sup>		0
2	HHV <sup>b</sup>		0
3	379.84681	199.91028	0.4490566
4	3404.778	6.4181	1.25
5	-58242.07809 for flue gas and -967670.773 for fly ash	211.0118484 for flue gas and 94.82284036 for fly ash	13.6593238
6	-867719.8627	214.4715163	0.467897

**2.3 Calculation of Chemical Exergy**

The chemical exergy of the solid fuel is calculated by using Eqs. (4.21), (4.22), and (4.23), and that for other state points by using Eqs. (4.9) and (4.10).The chemical exergy data for elements are taken from [27]. All these calculated value are tabulated in Table 6.

**Table 6** Chemical Exergy values on the state points.

State Points	Chemical Exergy (GJ/hr) for Baseline Coal Only	Chemical Exergy (GJ/hr) for 15% Co-firing
1	1041.13	895.6882
2	--	172.3145
3	0	0

4	0.04212	0.04212
5	37.76015671	36.802
6	0.573048	0.632

## 2.4 Total Exergy Calculation

The total exergy is the summation of physical exergy and chemical exergy. The total exergy for base coal line and 15% co-firing at all state points are tabulated in Table 7

**Table 7** Total Exergy values on the state points

State Points	Total Exergy (GJ/hr)	
	Baseline Coal Only	15% Co-firing
1	1041.13	895.6882
2	--	172.3145
3	0.44	0.45

$$\dot{E}_i(\text{coal}) = 1041.13 + 0 + 0.44262 - 360.0 - 269.7364567 - 1.153296 = 410.68 \text{ GJ/hr}$$

$$\begin{aligned} \dot{E}_L(\text{Co-firing}) &= 895.6882 + 172.315 + 0.4490566 - 360.0 - 50.4613238 - 1.099897 \\ &= 656.89 \text{ GJ/hr} \end{aligned}$$

From the above calculated value of exergy losses it is seen that the exergy losses for the co-firing option is more than that of baseline coal. Since from the energy balance data for the plant shows the stack gas loss 97.6 GJ/hr, boiler radiation losses 3.4 GJ/hr, unburned carbon loss 5.5 GJ/hr, unaccounted for boiler heat loss 16.4 GJ/hr for coal only and that of 15% co-firing are 112.1 GJ/hr, 3.4 GJ/hr, 4.4 GJ/hr, and 16.6 GJ/hr, respectively, this exergy losses corresponding to these energy losses are included in the above calculated exergy loss values for both the cases.

## 3. CONCLUSIONS

Based on the obtained results presented in this dissertation, the following important inferences can be drawn:

- The chemical exergy of fuel in case of biomass co-firing is more than that of coal-only case by 2.58%.
- The total exergy value of flue gas with fly ash in case of biomass co-firing is less by 81.29% compared to that of baseline coal case.
- The total exergy value of bottom ash in case of biomass co-firing is less by 4.63% compared to that of baseline coal case.
- The exergy losses including irreversibility losses are more for biomass co-firing by 59.95% as compared to coal-only case.
- The available energy losses through emission products, like fly ash, bottom ash, etc., can be

4	1.292087	1.29212
5	269.7364567	50.4613238
6	1.153296	1.099897

## 2.5 Exergy Losses

The exergy losses, in general, can be written as

$$\dot{E}_L = \dot{E}_1 + \dot{E}_2 + \dot{E}_3 - \dot{P} - \dot{E}_5 - \dot{E}_6$$

Using the above calculated value of exergy rate at state points the exergy losses for base coal and 15% co-firing, respectively, are:

- comprehensively reduced by co-firing biomass in a coal fuel based power plant.
- Since total irreversibility losses including exergy losses corresponding to the unaccounted boiler heat losses is more in case of biomass co-firing compared to that of baseline coal case, the biomass co-firing is not an acceptable option for prolong use.
- Considering environmental friendliness to certain extent, the biomass co-firing option in coal fuel based power plants can be considered as a short-term stop-gap measure to reduce environmental pollution. It may continue till some technologically sound and cost effective measures of CO<sub>2</sub> sequestration options are available for the coal based thermal power plants.

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